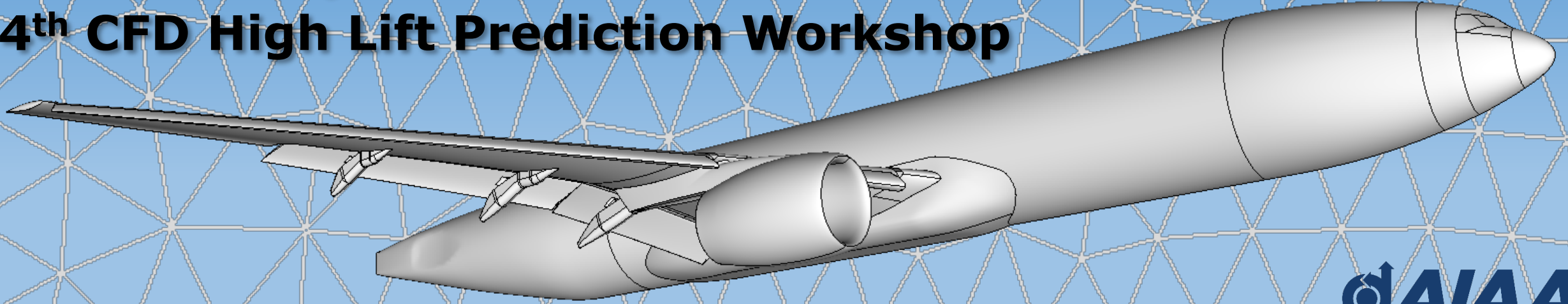


**3<sup>rd</sup> Geometry and Mesh Generation Workshop**  
**4<sup>th</sup> CFD High Lift Prediction Workshop**



# **HO-TFG Meshing & Solution**

**Marshall Galbraith (MIT)**

**Steve Karman (Oak Ridge National Laboratory)**

# Terminology

- Mesh order is referenced by the polynomial degree of the basis function
  - Q1 (linear, e.g. standard mesh)
  - Q2 (quadratic)
  - Q3 (cubic)
  - Q4 (quartic)
- Finite Element solution order is referenced using a similar convention
  - P1 is 2<sup>nd</sup> order solution
  - P2 is 3<sup>rd</sup> order solution
- P1Q2-FV and P2Q2-FV are 2nd and 3rd-order Finite-Volume discretizations that couple the solution on curved Q2 Primal and Dual meshes

# Demographics Mesh Generation

## TFG ID/Name

G = Geometry  
R = RANS  
A = Adaptation  
H = High-order  
L = Hybrid RANS/LES  
W = WMLES/LB



TFG Name	HO
Number of Active Participants (current)	~12
Number of Observers (current)	~10

Group Submissions Received	Members (Org)	Tools Used (Geom/Grid/Solver), by name	Participation
H-001	ORNL (Pointwise)	Pointwise, HP_CurveMesh	HLCRM (Q2), Juncture Flow Model (Q2)
H-003	GridPro	GridPro	2D-HLCRM (Q2), Juncture Flow Model (Q2)
H-006	INRIA	ho-feflo.a	HLCRM (Q2)
H-019	Barcelona Sup. Cent.	Pointwise, ParCur	HLCRM (Q2)

# Demographics Solver

TFG Name	HO
Number of Active Participants (current)	~12
Number of Observers (current)	~10

## TFG ID/Name

G = Geometry  
 R = RANS  
 A = Adaptation  
 H = High-order  
 L = Hybrid RANS/LES  
 W = WMLES/LB



Group Submissions Received	Members (Org)	Tools Used (Geom/Grid/Solver), by name	Participation
H-004	MIT	SANS	RANS-SA: 2D-HLCRM(Q2) P1-P2 SUPG/VMSS Adapt
H-005	ORNL, UTK, DoD CREATE-AV	COFFE	RANS-SA: 2D-HLCRM(Q2) P1-P2 SUPG
H-012	ONERA / DAAA	HO_DualMaker(Q2), Nextflow_ITW	URANS-SA: 2D-HLCRM(Q1) P2, HLCRM(Q2) P1
H-023*	Boeing	GGNS	RANS-SA: HLCRM(Q2) P2
H-013	Princeton	maDG	ILES: HLCRM(Q1) P1-P3 DG
W-047	U Kansas	HpMusic	WMLES: HLCRM(Q2) P2 Flux Reconstruction
H-021	Tecplot	Tecplot	Solution visualization for high-order FEM

\*Late submission

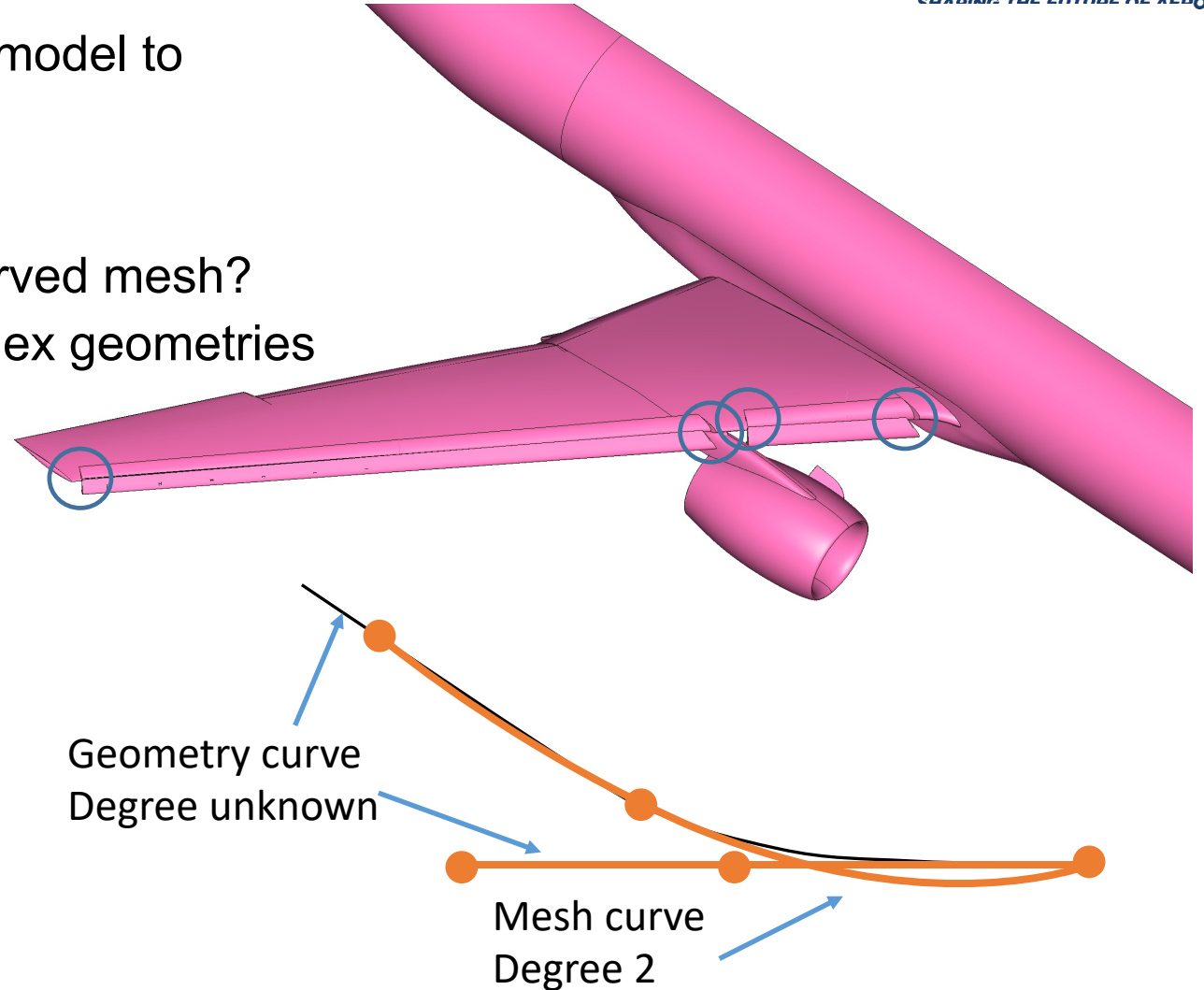
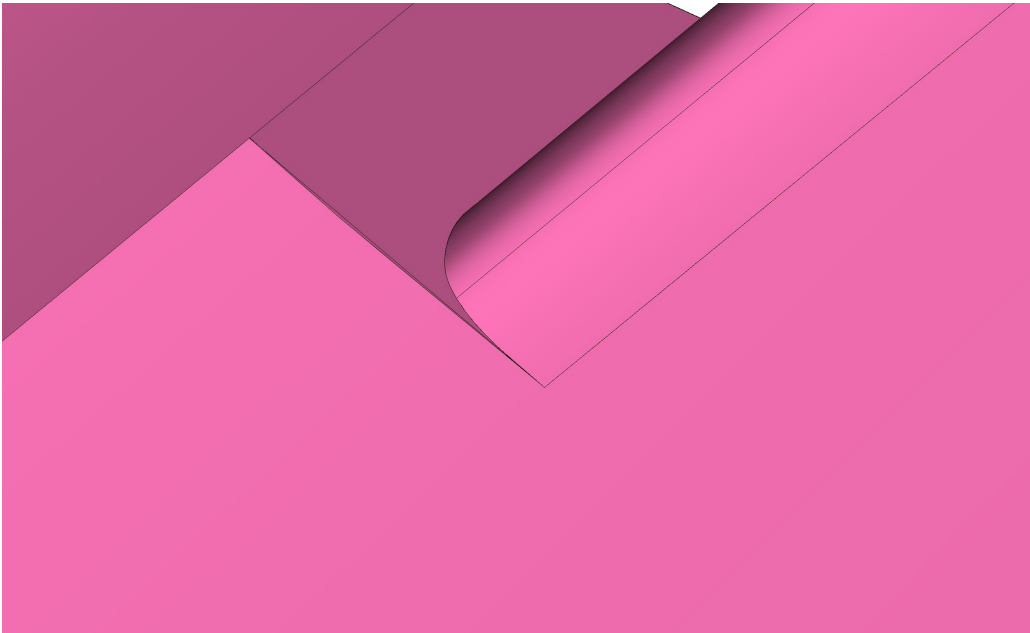


# Key Questions

#	Key Question	By Which Groups (PID)	Adequately answered with supporting evidence?
1	Can 3D curved Q2/Q3 meshes be generated for the HL-CRM?	H-001, H-006, H-019	Yes
3	What mesh quality metrics are used to evaluate high order meshes?	H-001, H-019	Yes
4	How well do the curved meshes conform to the actual geometry?	H-001, H-019	Yes
5	Can high-order FEM/FV schemes be used with the HL-CRM configuration?	H-012, H-013, H-023	Partially
6	What are the Y+ normal distance requirement for LES/WMLES with high order finite element schemes?	H-013	Partially

# Geometry/Meshing Trouble Spots

- Pinch points were “fixed” in the geometry model to eliminate cross-over.
  - Curving process (Q2) still had issues.
- Should we modify the geometry or the curved mesh?
- Virtual geometry and quilts help for complex geometries



# Meshing Findings/Lessons Learned



- A supplemental HO Mesh Generation Guidelines document was created that extended the meshing parameter sets in the coarser direction, adding AA, AAA and AAAA and eliminated E and F from the tables.
- Initial AAAA meshes were generated and curved using Pointwise
  - Most participants lacked computer resources to run these meshes
- A new series was created (Coarse, Medium, Fine and Extra Fine)
  - The coarsest mesh was the smallest mesh possible, maintaining geometry integrity.
- Participants experimenting with HO-WMLES algorithms.
  - Curved meshes generated with increased normal distances ( $Y^+$  values of 10, 50, 100, 200, 800 based on Pointwise  $Y^+$  calculator)

# Meshing Findings/Lessons Learned



- Curved 2D meshes were generated with H-003 and H-002
- H-001 and H-003 generated curved meshes for the Juncture Flow Model case (no solutions were attempted, a meshing-only exercise).
- H-001 and H-019 (CRM-HL)
  - Linear meshes were generated and curved
- H-006 (CRM-HL)
  - Started with the Pointwise linear meshes and generated curved meshes
- H-012 (CRM-HL)
  - High-order Dual meshes generated with HO\_DualMaker starting with Pointwise Q2 meshes

# Meshing Findings/Lessons Learned



- The most importance quality metric is the Jacobian, which can vary within a high-order element
  - The curving with viscous clustered meshes must ensure positive Jacobians (mesh validity)
  - Scaled Jacobian and relative shape distortion are used to check the mesh quality
- Shape conformity is an important metric that measures the error between the curved mesh and the geometry shape
- Finer mesh around nacelle on Q2 Coarse mesh greatly improved WMLES solution

# Shape Conformity

H-001: Medium mesh. Selected body components.  $Y^+ \sim 1$

Body	Max. Error		Avg. Error	
	Q1	Q2	Q1	Q2
Fuselage	1.27	0.21	0.11	2.6e-3
Nacelle	0.37	4.9e-2	0.023	4.6e-4
Wing	0.26	3.6e-2	5.7e-3	1.9e-4

H-019: Medium mesh. Full vehicle.  $Y^+ \sim 100$

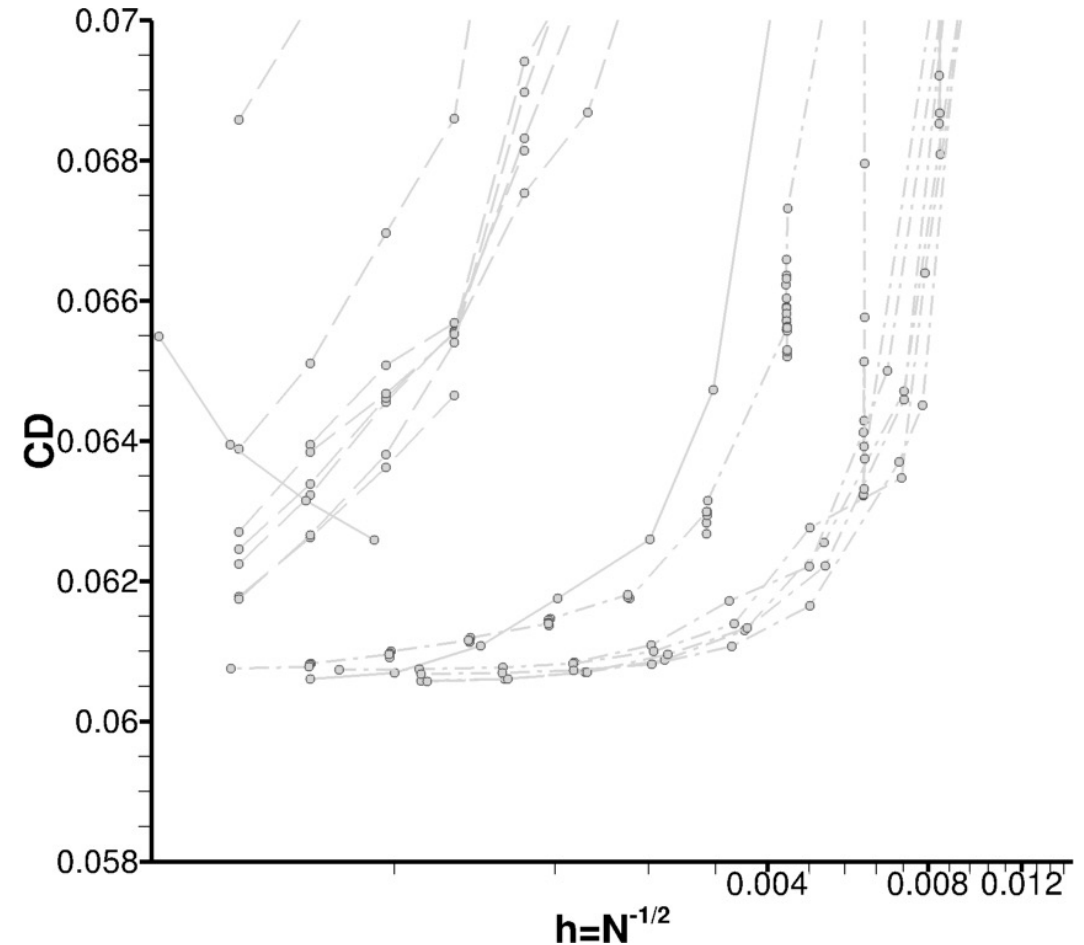
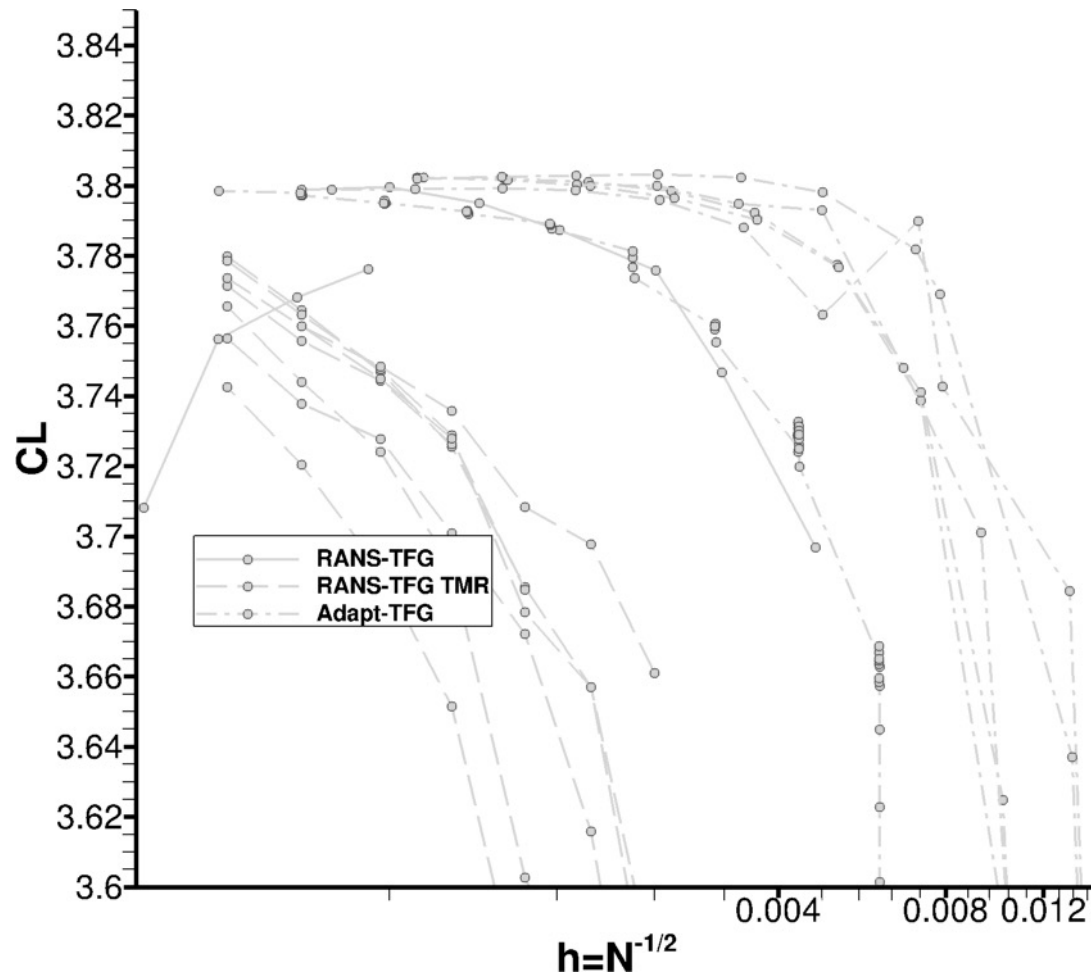
Body	Max. Error			Avg. Error		
	Q1	Q2	Q3	Q1	Q2	Q3
Full Vehicle	1.48	0.25	0.12	0.1	9.8e-4	2.9e-4

# High-Order Case3 RANS-SA

- **H-005:** FEM implicit steady RANS
  - GridPro(P1Q1, P2Q2), and TMR(P1Q1) meshes
- **H-004:** (MIT): FEM implicit steady RANS
  - GridPro(Q2), TMR(Q1), and Adapted(Q3) meshes with P1 and P2
- **A-013:** (MIT): FEM implicit steady RANS
  - TMR(Q1), and Adapted(Q1), meshes with P1
- **H-012:** FV time-implicit URANS, explicit pseudo-time solver
  - GridPro (Q2) P2
  - Time averaged solutions for lift and drag

# Basic CFD Results Case3

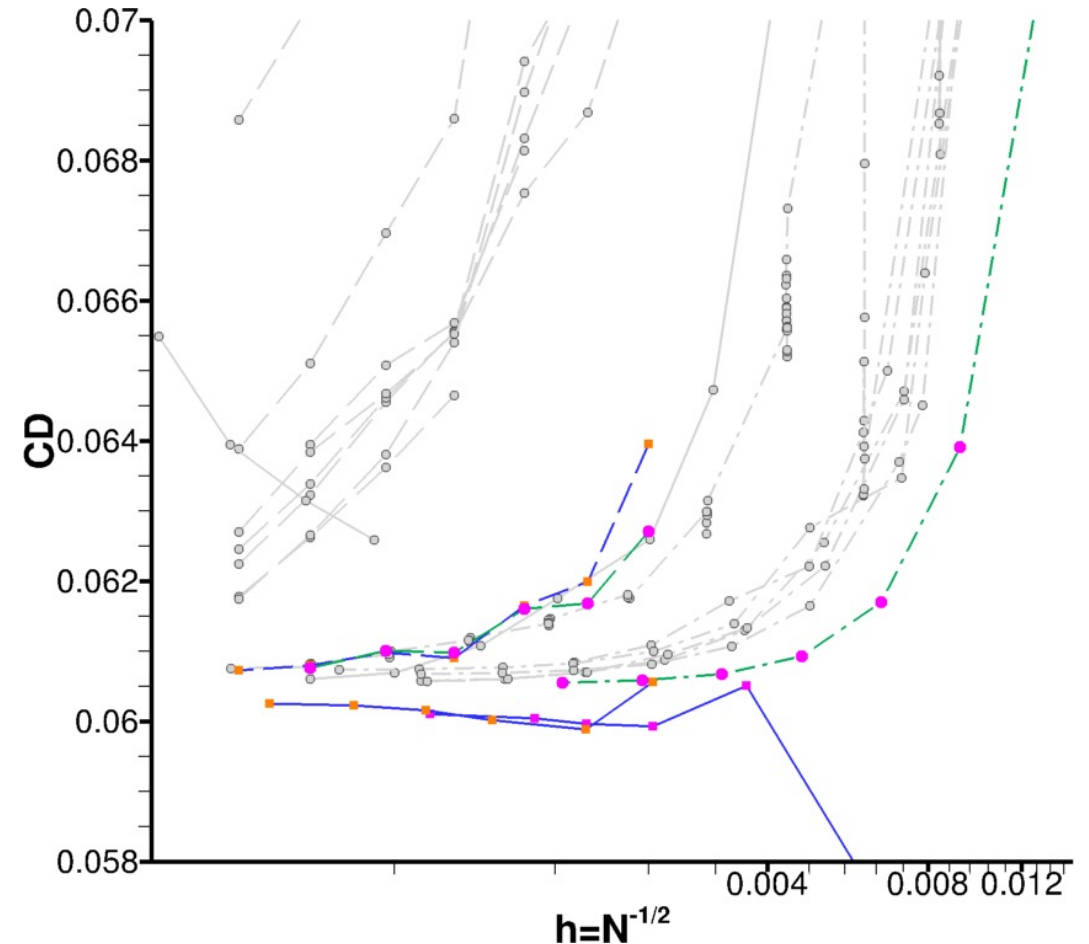
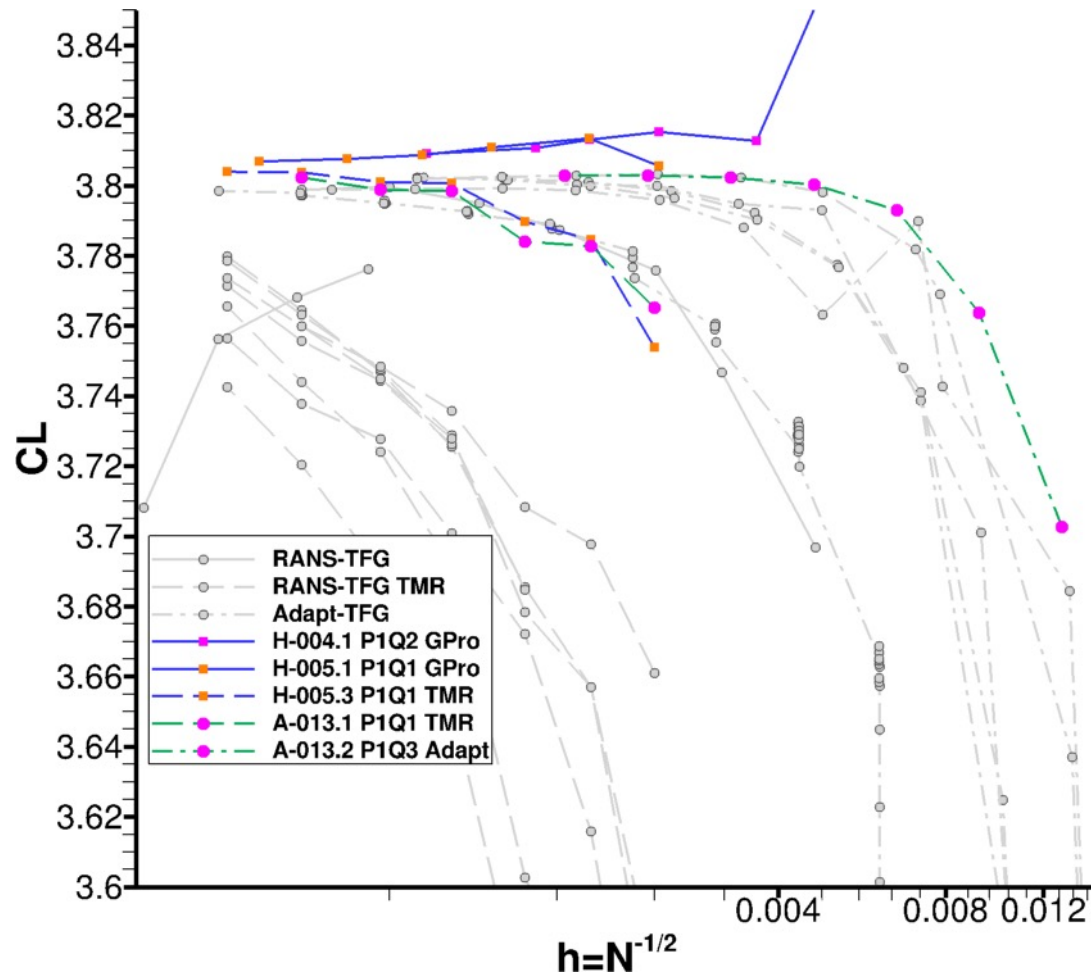
2D CRM Airfoil Lift and drag convergence with degree of freedom refinement: RANS-SA





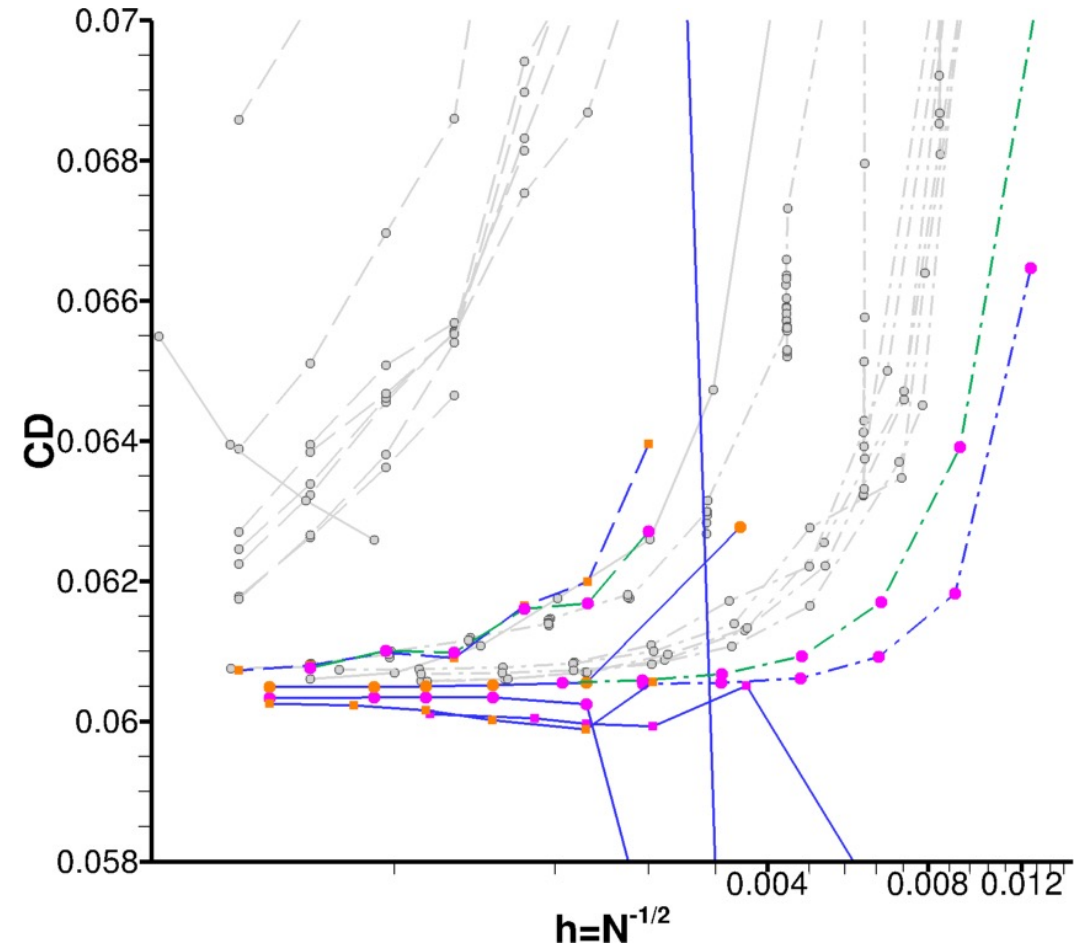
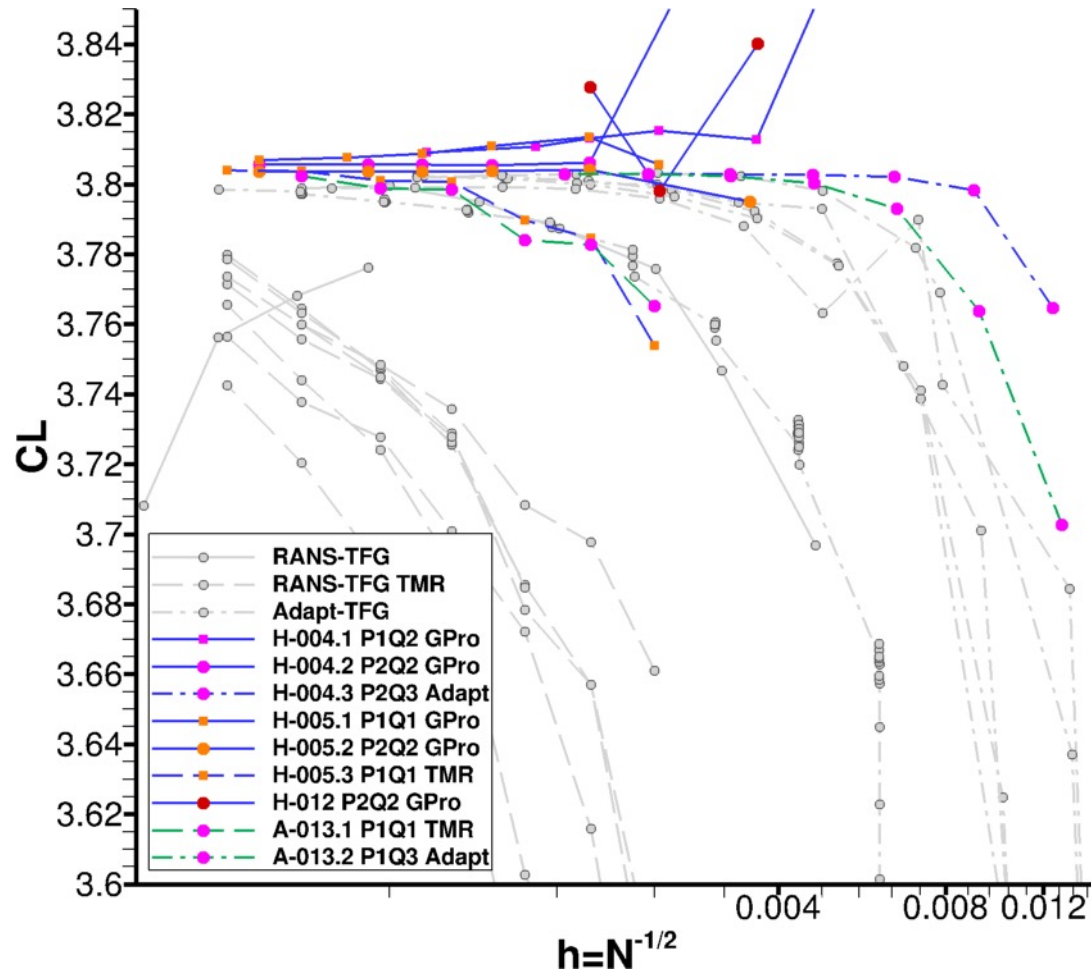
# Basic CFD Results Case3

2D CRM Airfoil Lift and drag convergence with degree of freedom refinement: RANS-SA



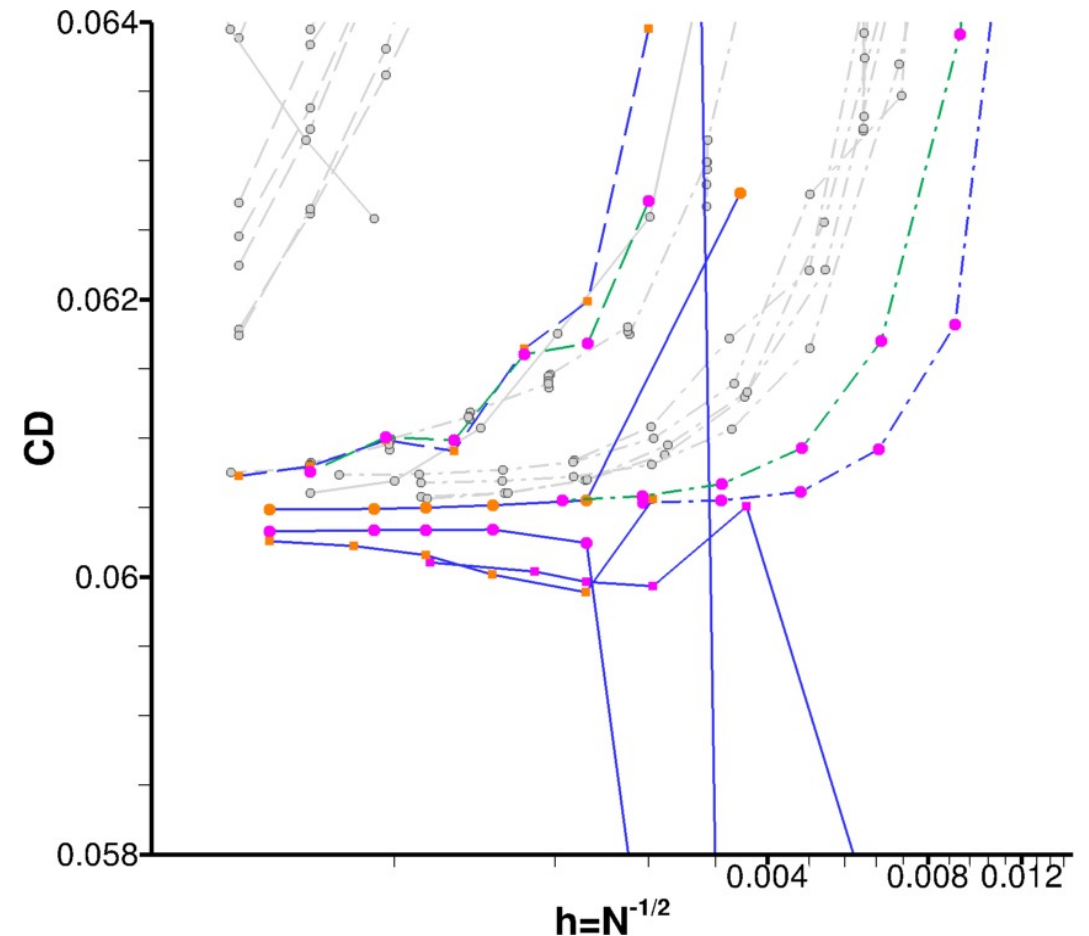
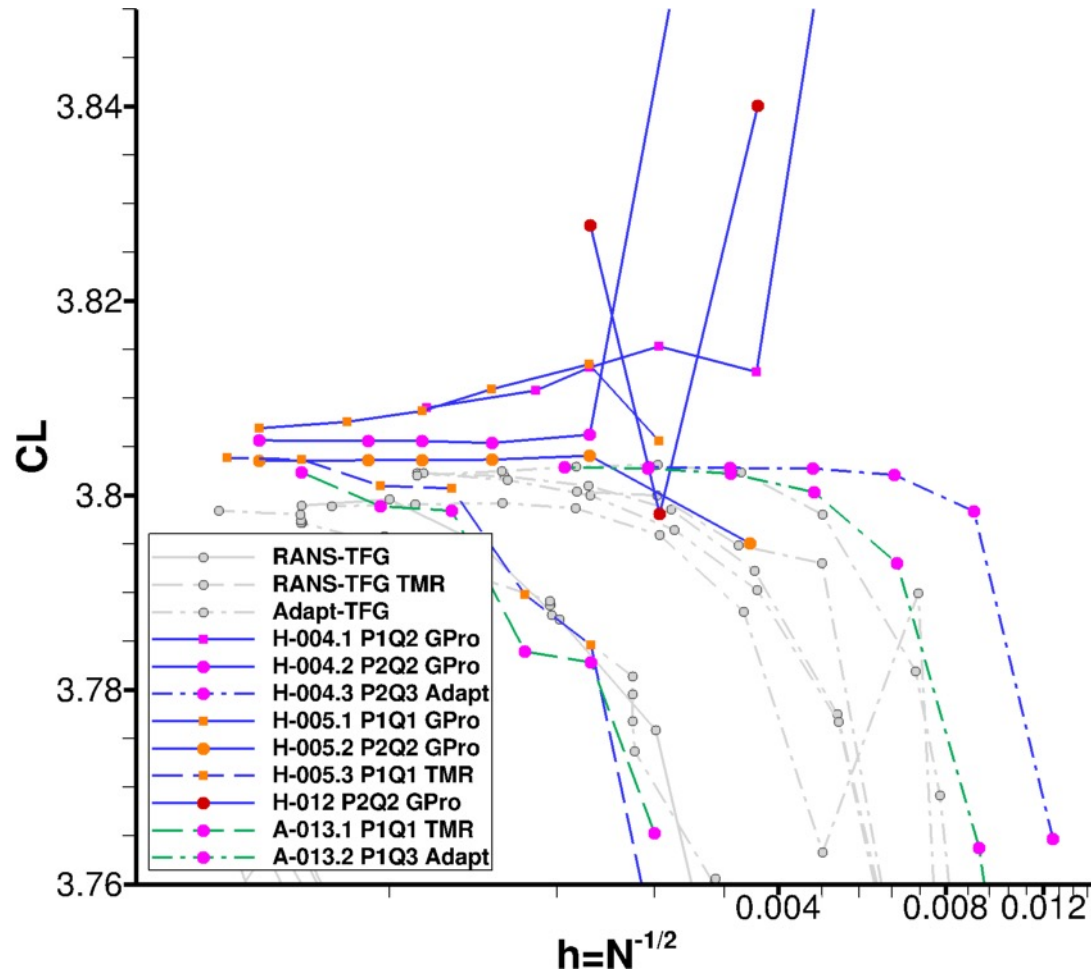
# Basic CFD Results Case3

2D CRM Airfoil Lift and drag convergence with degree of freedom refinement: RANS-SA



# Basic CFD Results Case3

2D CRM Airfoil Lift and drag convergence with degree of freedom refinement: RANS-SA



# High-Order Case1b and Case2a

## H-012

- P2 FV, k2 reconstruction
- RANS-SA
- **Explicit time stepping**
- Q2 mesh 2 to 21M mixed  
Pointwise Coarse to Medium  
Various  $Y^+$  : 100 to 800
- Coupled solver :
  - cell-center + cell-vertex (2G)
  - cell-center + cell-vertex + cell-edge (3G)
  - cell-center + cell-vertex + cell-edge + cell-face (4G)

## H-013

- DG method in space
- BDF2 with GMRES
- No wall model
- Implicit LES ( $dt = 4.5e-5$ )
- **Q1** mesh 3M tet  
(Pointwise  $Y^+ = 100$ )
  - P1 12M DOF
  - P2 30M DOF
  - P3 60M DOF
- **$Re\ 0.5 \times 10^6$**

## W-047

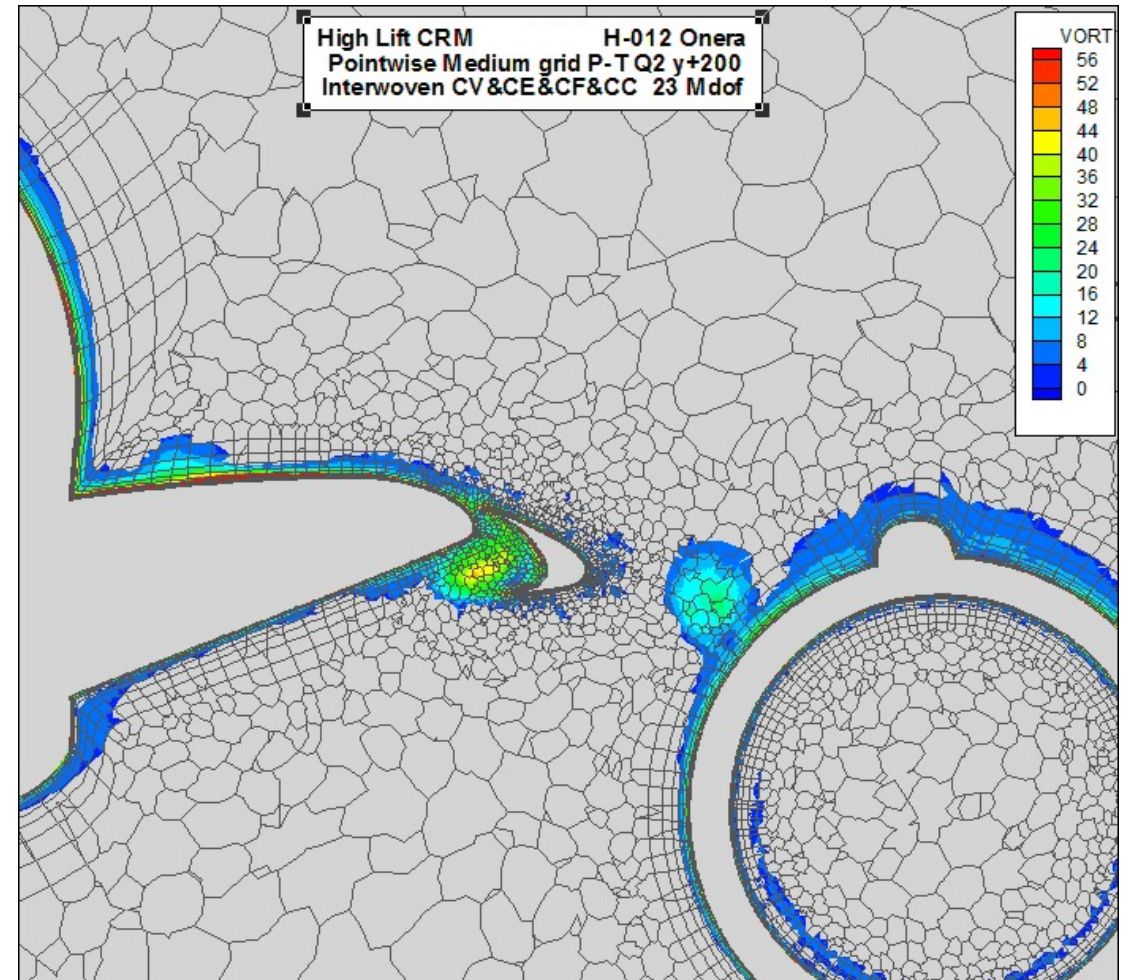
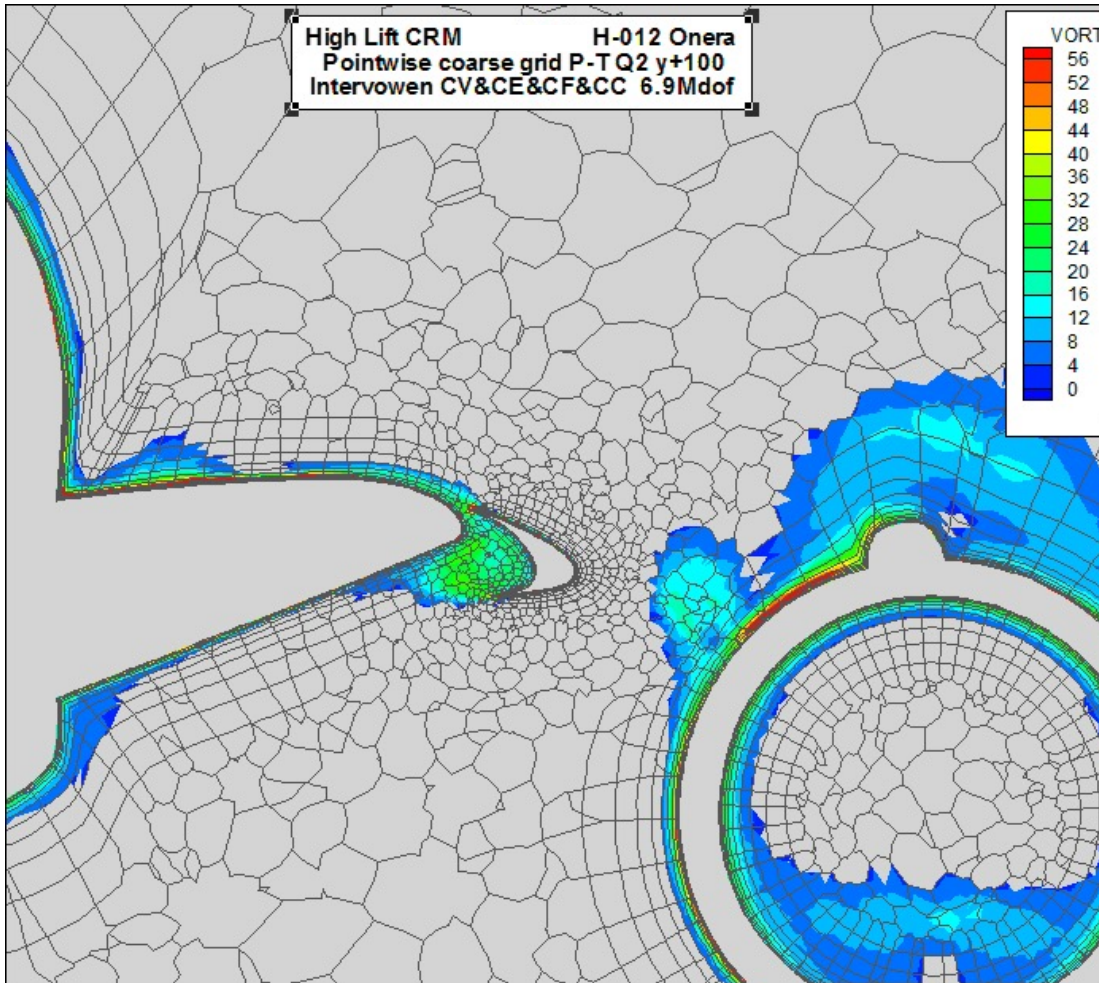
- P1 and P2 FR/CPR
- BDF2 with GMRES
- Equilibrium wall-model
- Implicit LES
- Q2 mesh 1.02M mixed  
(Pointwise  $Y^+ = 800$ )
  - P1 4.8 M DOF
  - P2 13.2 M DOF
  - Equivalent  $Y^+ \sim 200$ -260 near the wall  
( $\sim 7mm$ )

## H-023

- P2 SUPG
- RANS SA-neg
- Fully implicit GMRES
- Q2 mesh 6M tet (Pointwise  $Y^+ = 200$ )
  - P2 7.8M DOF

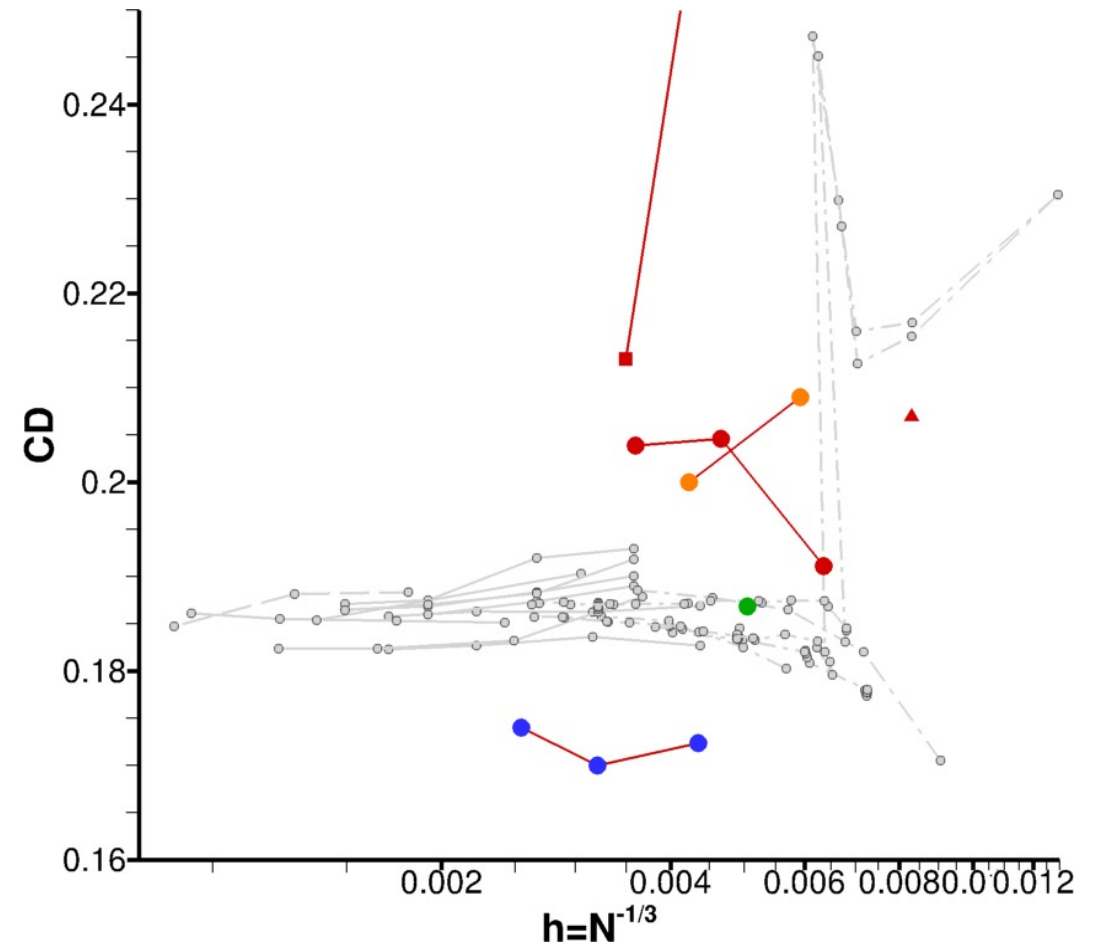
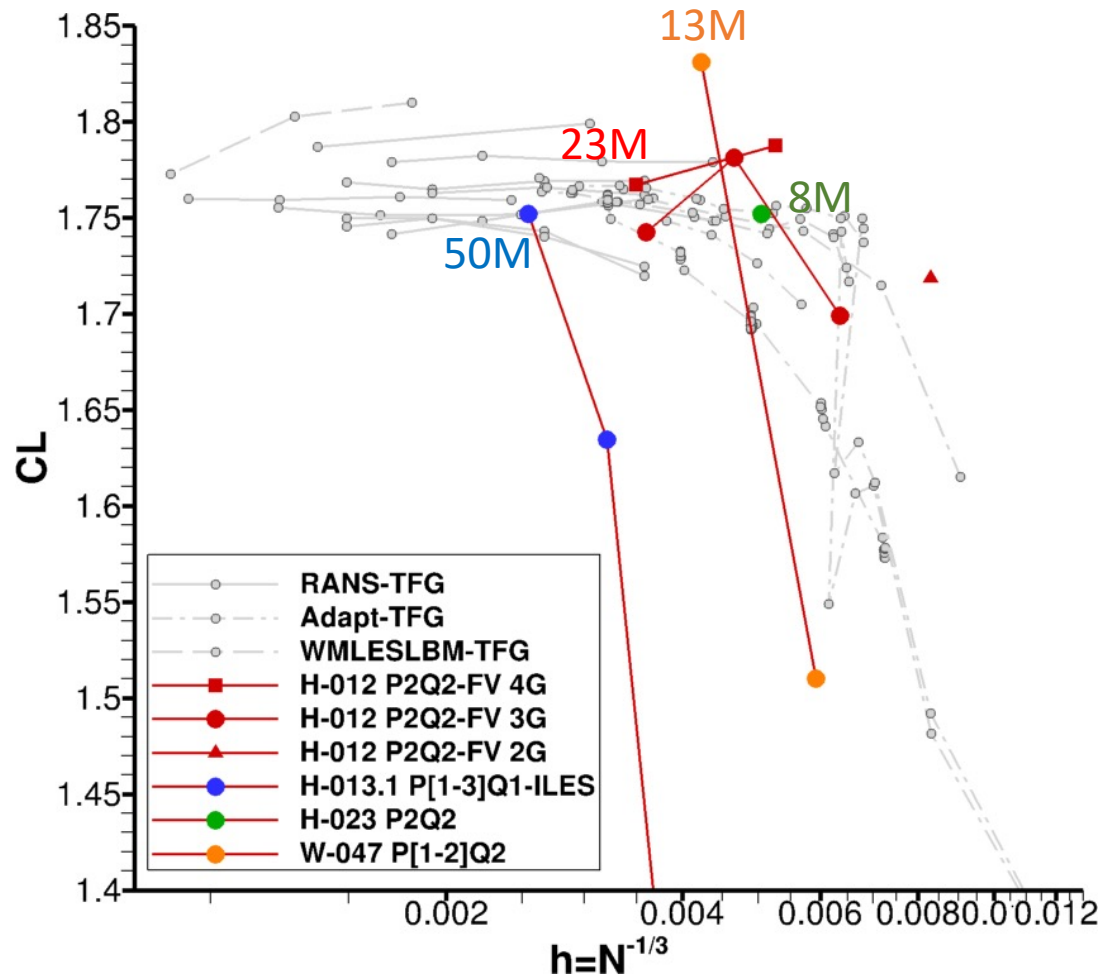


# H-012: URANS (7.05 AoA) View 11 on Cell-Vertex Grid Refinement Effect



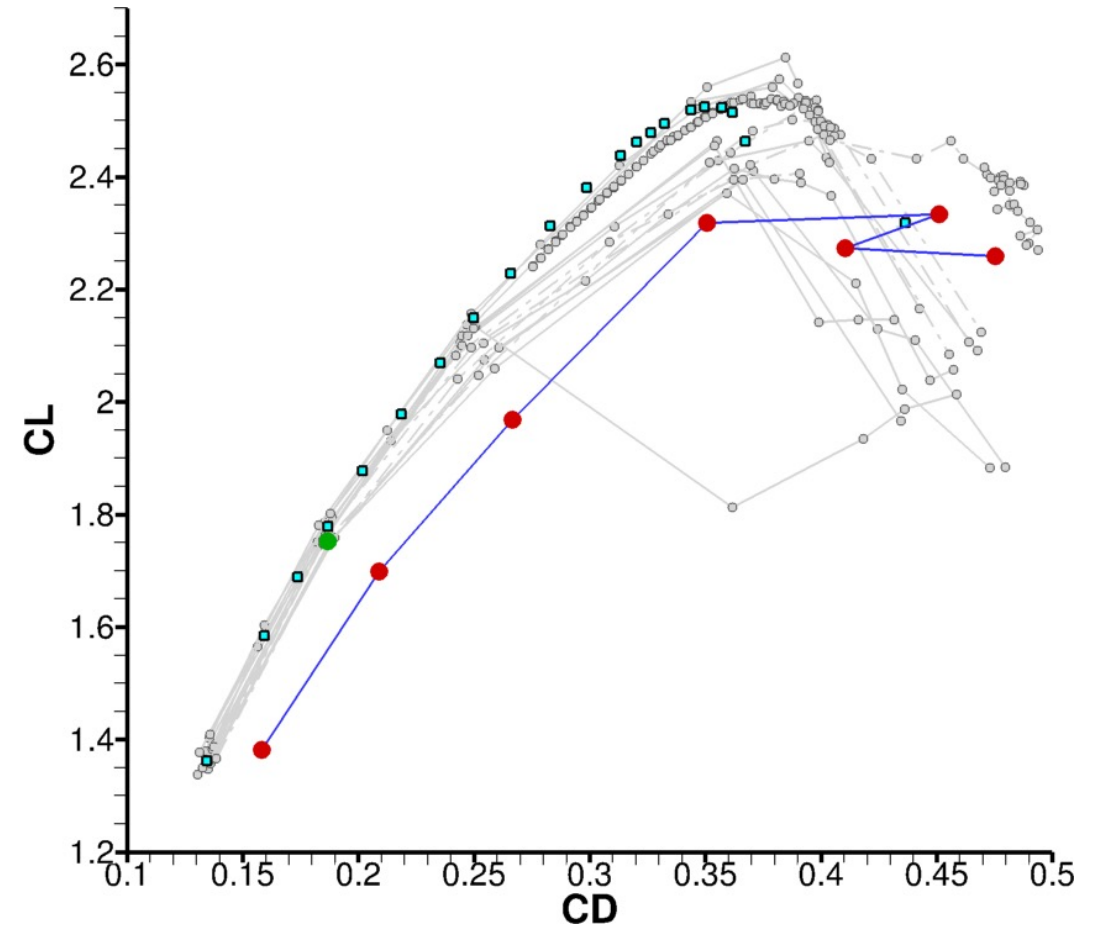
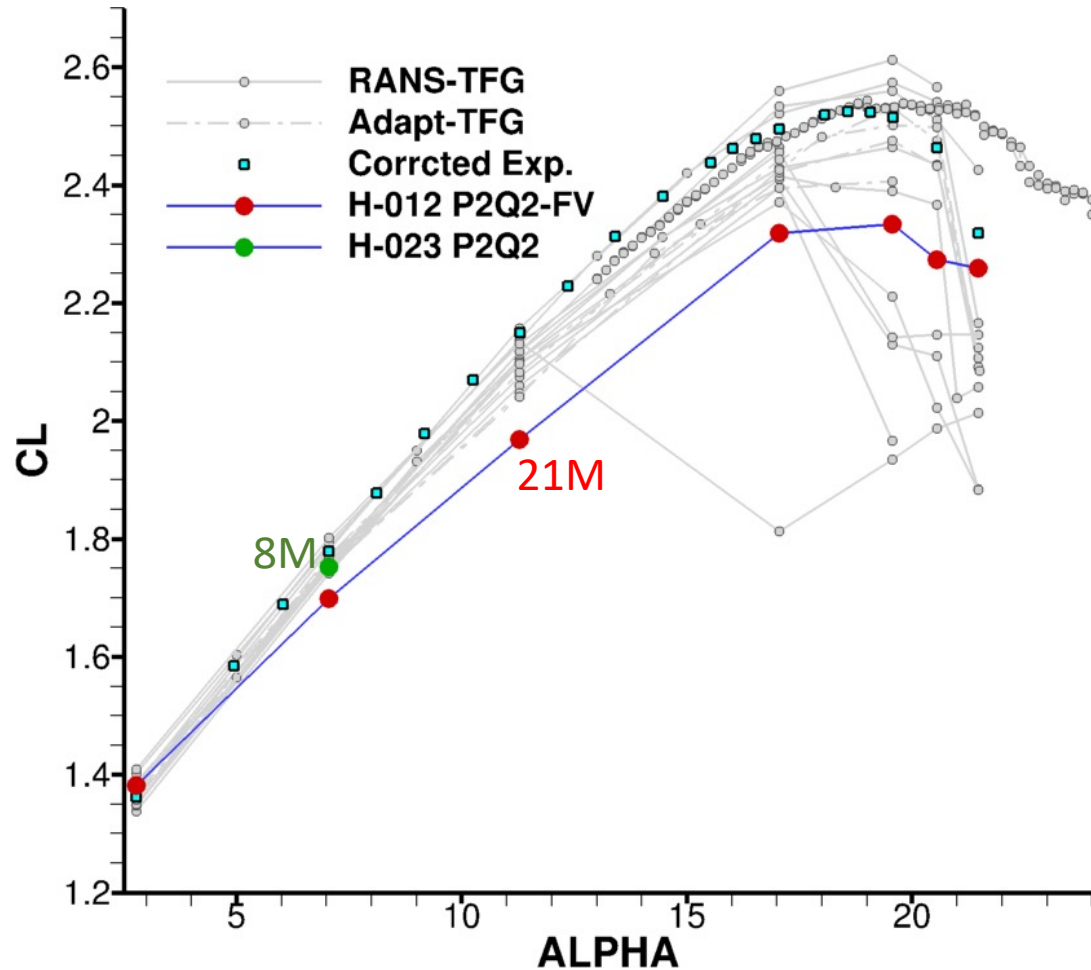
# Basic CFD Results Case1b

Lift and drag convergence with degree of freedom refinement



# Basic CFD Results Case2a

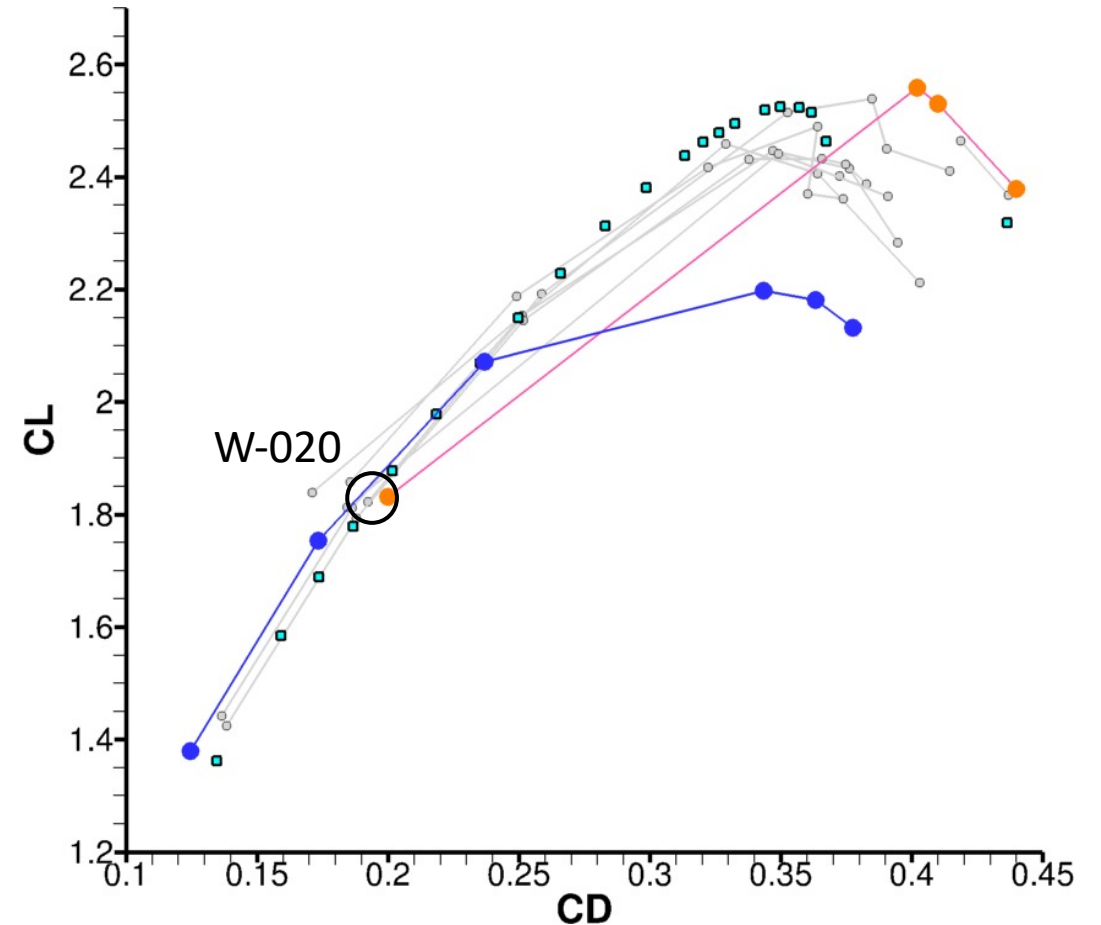
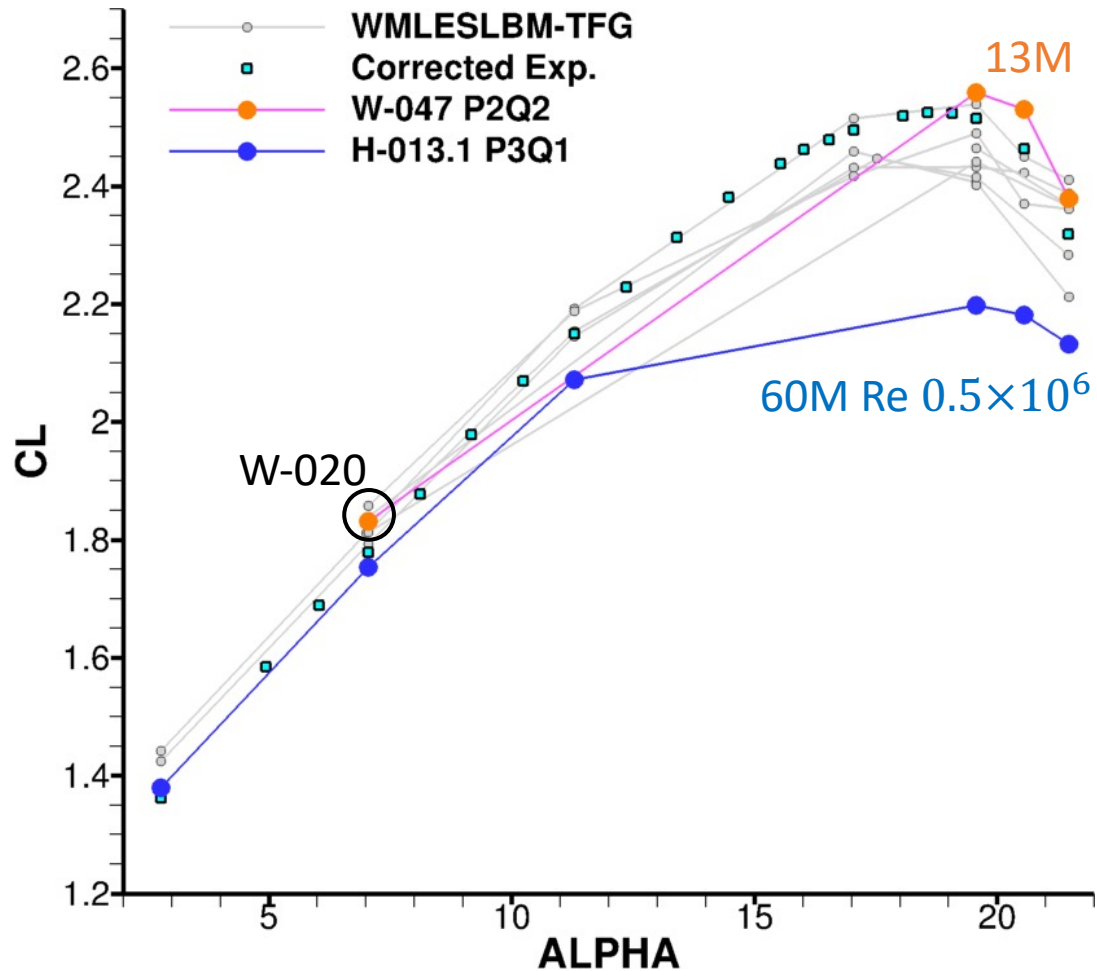
Lift curve ( $CL-\alpha$ ), drag polar ( $CL-CD$ ): RANS-SA





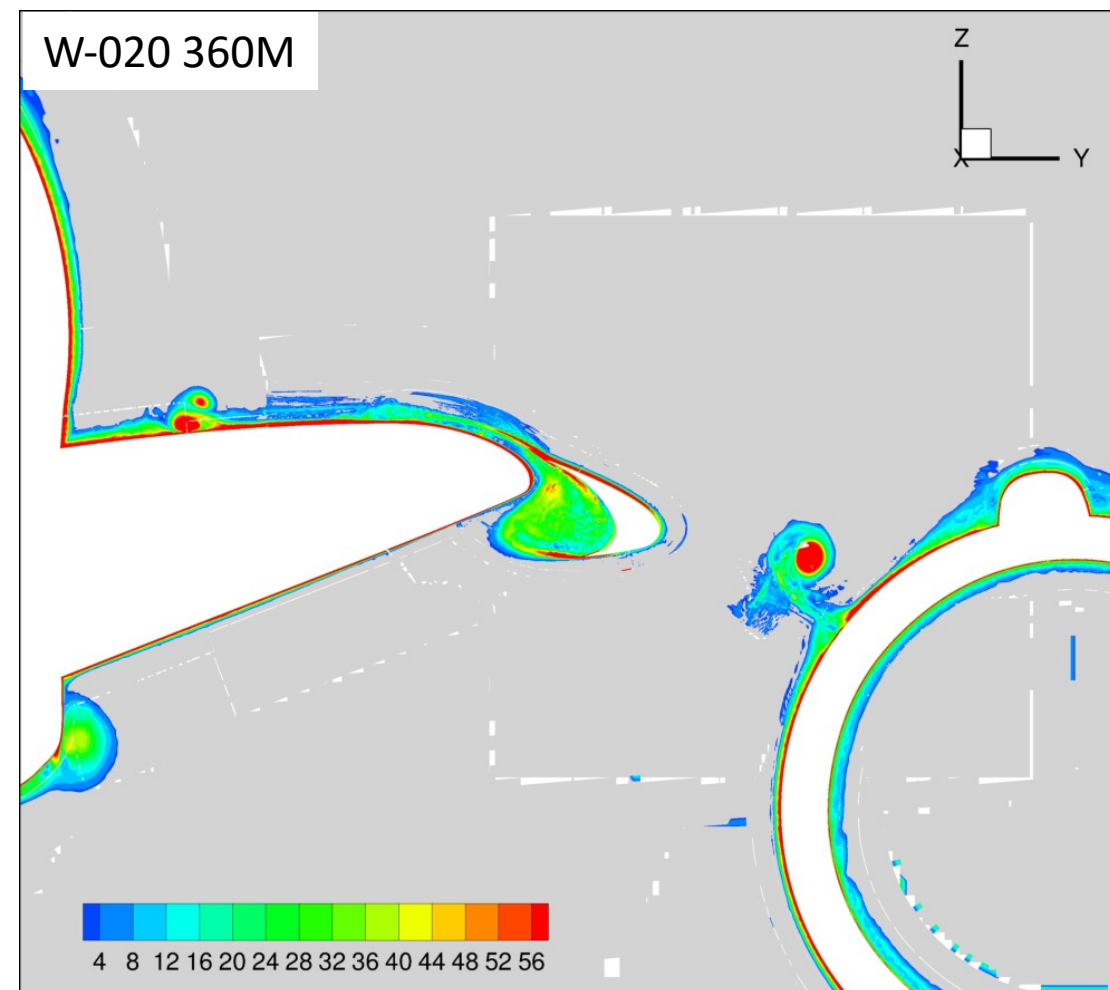
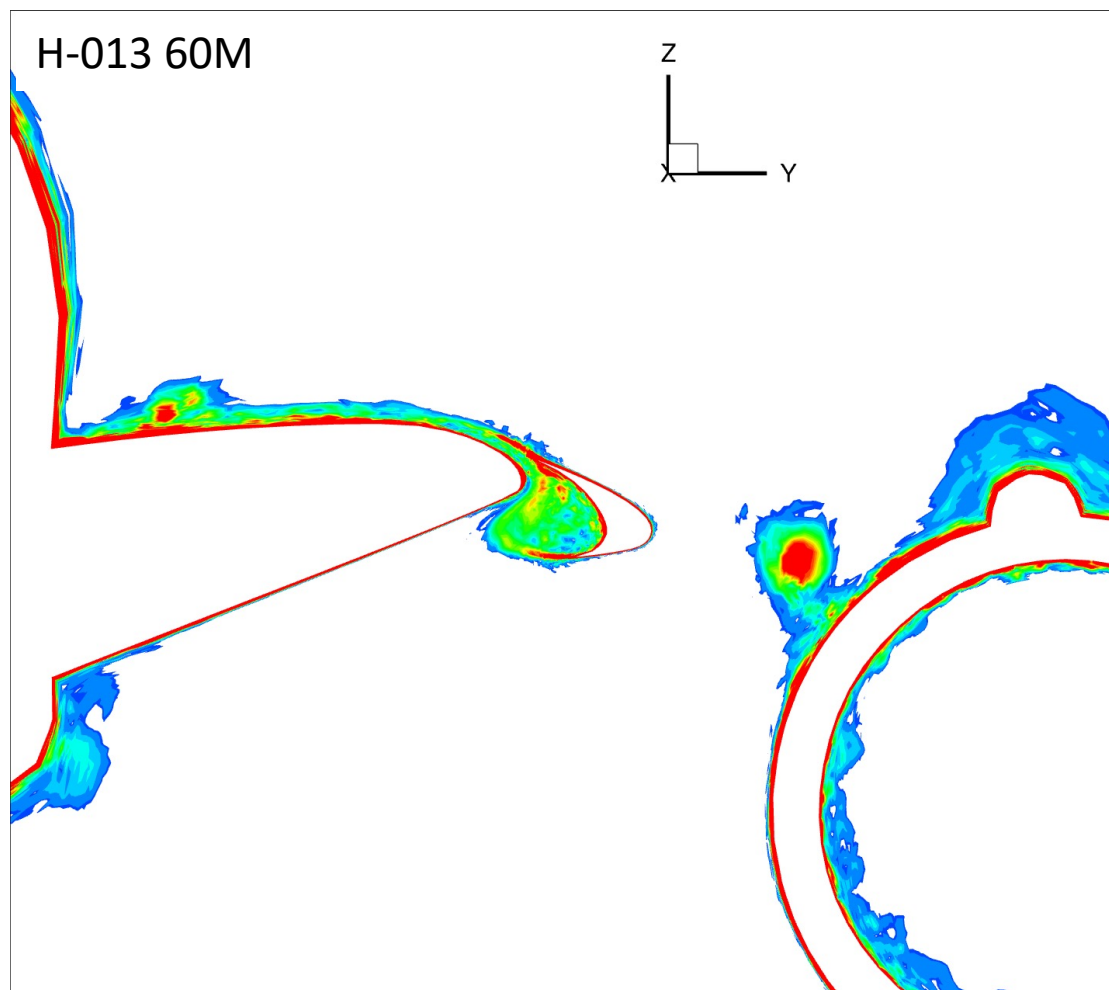
# Basic CFD Results Case2a

Lift curve ( $CL-\alpha$ ), drag polar ( $CL-CD$ ): LES



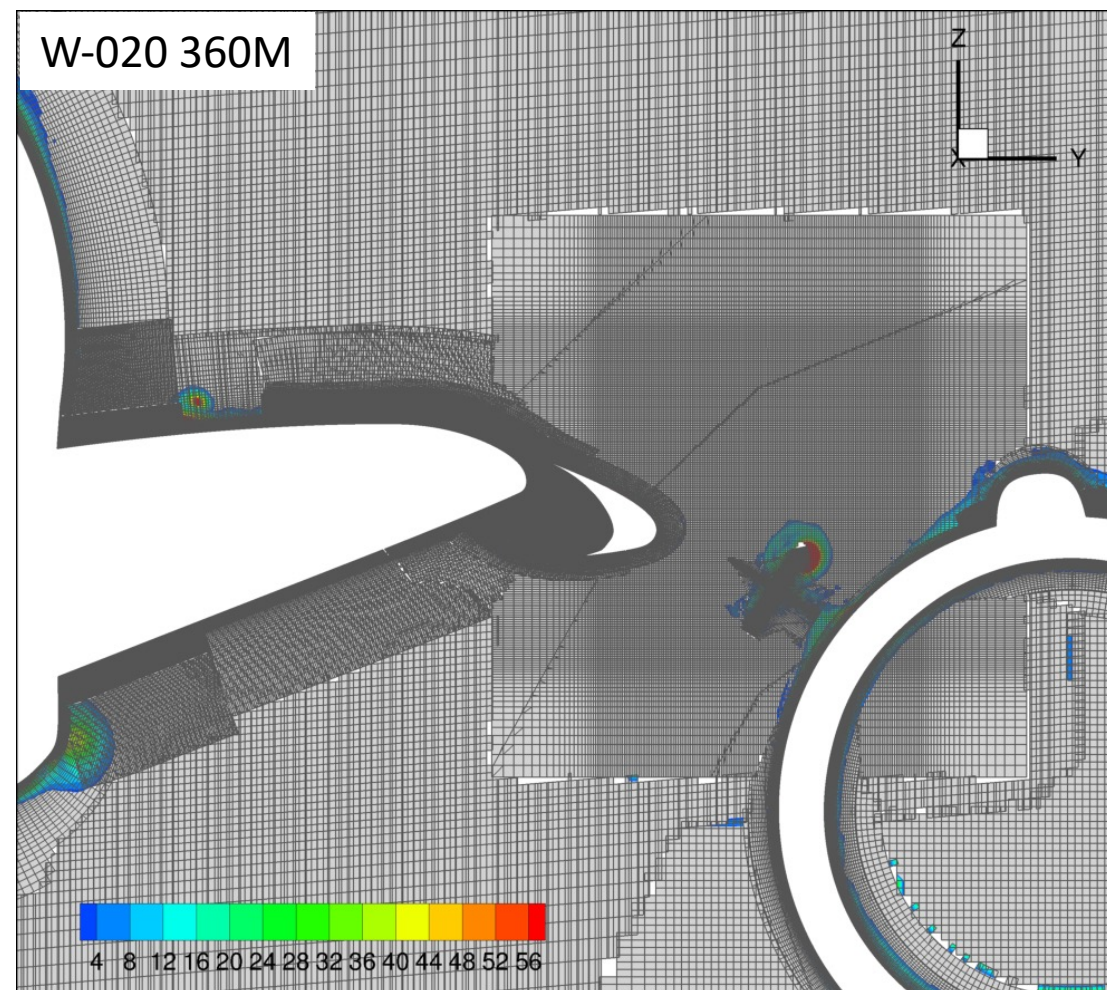
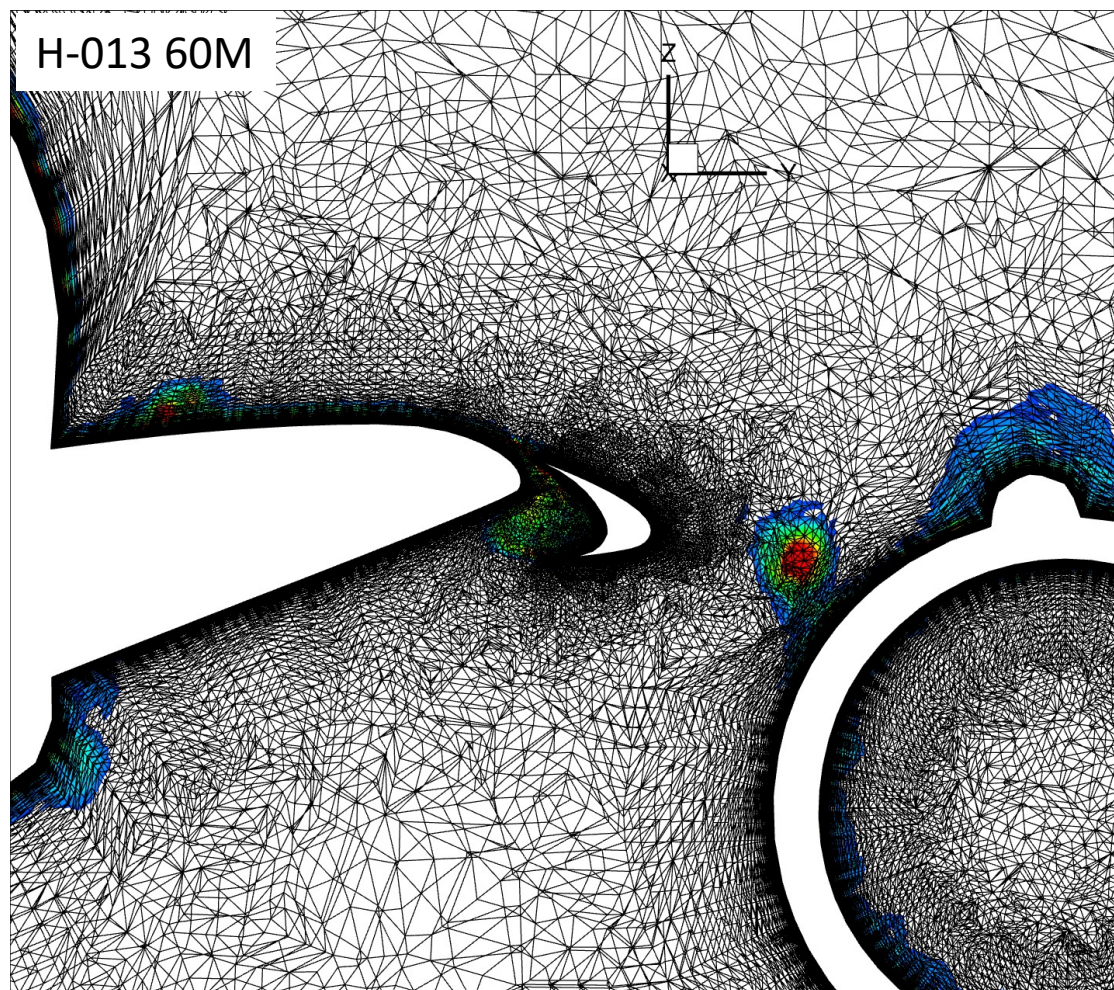


# ILES (7.05 AoA) View 11



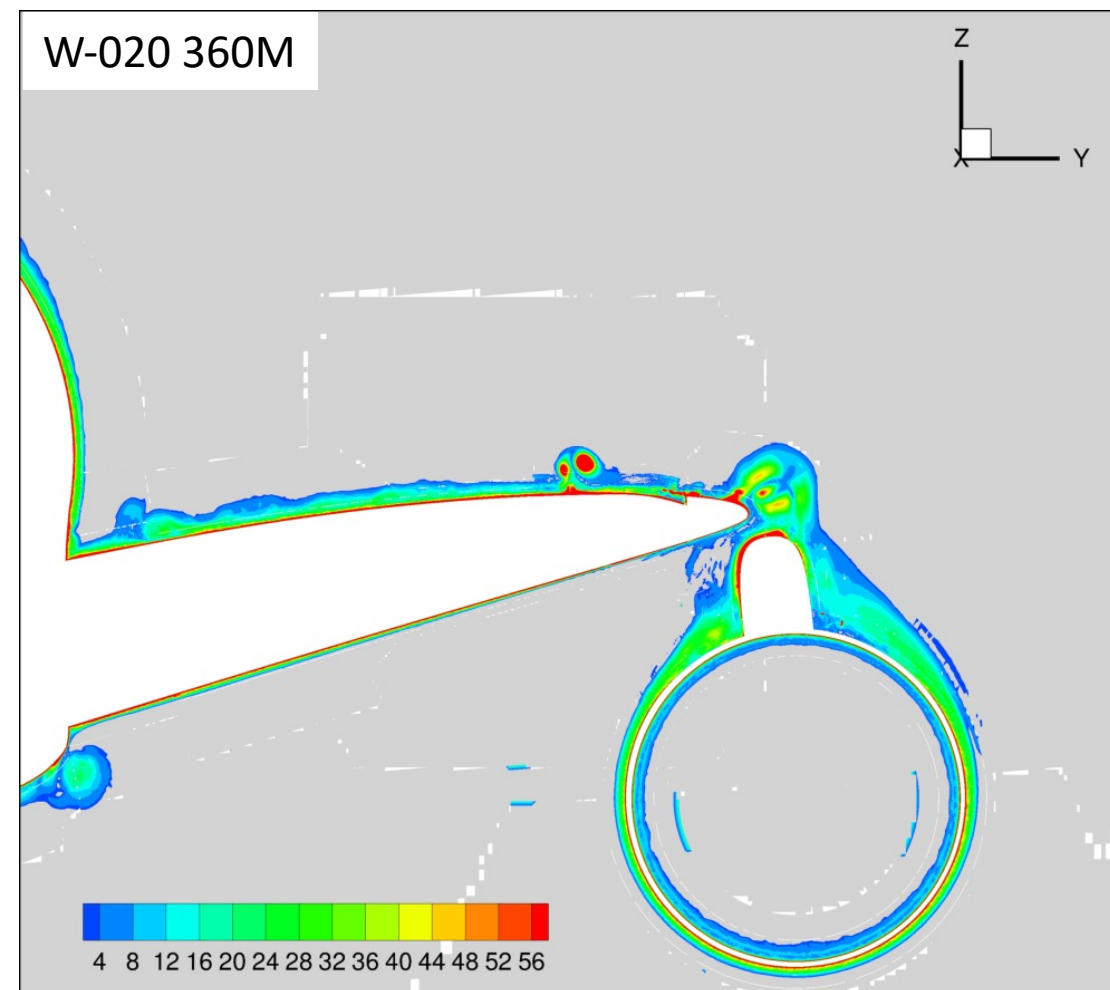
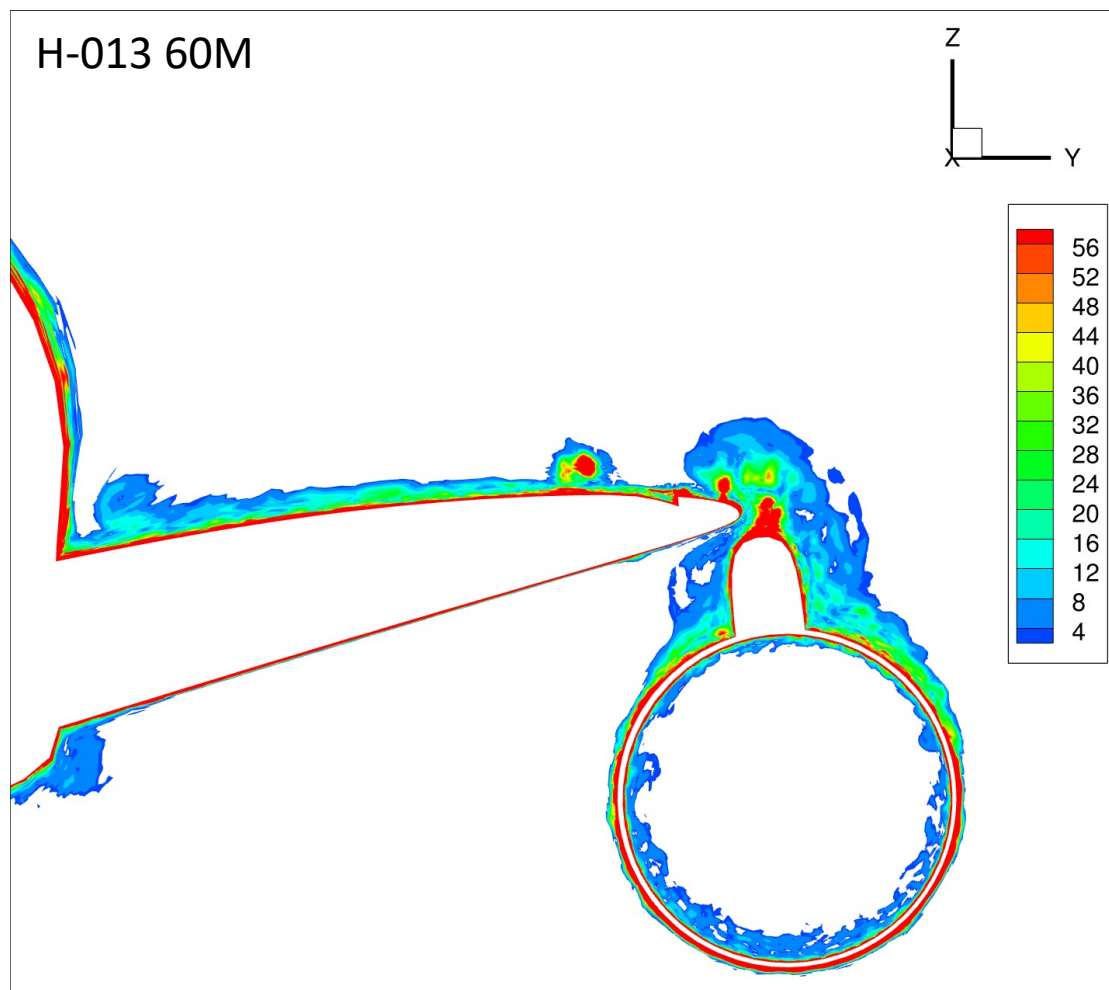


# ILES (7.05 AoA) View 11



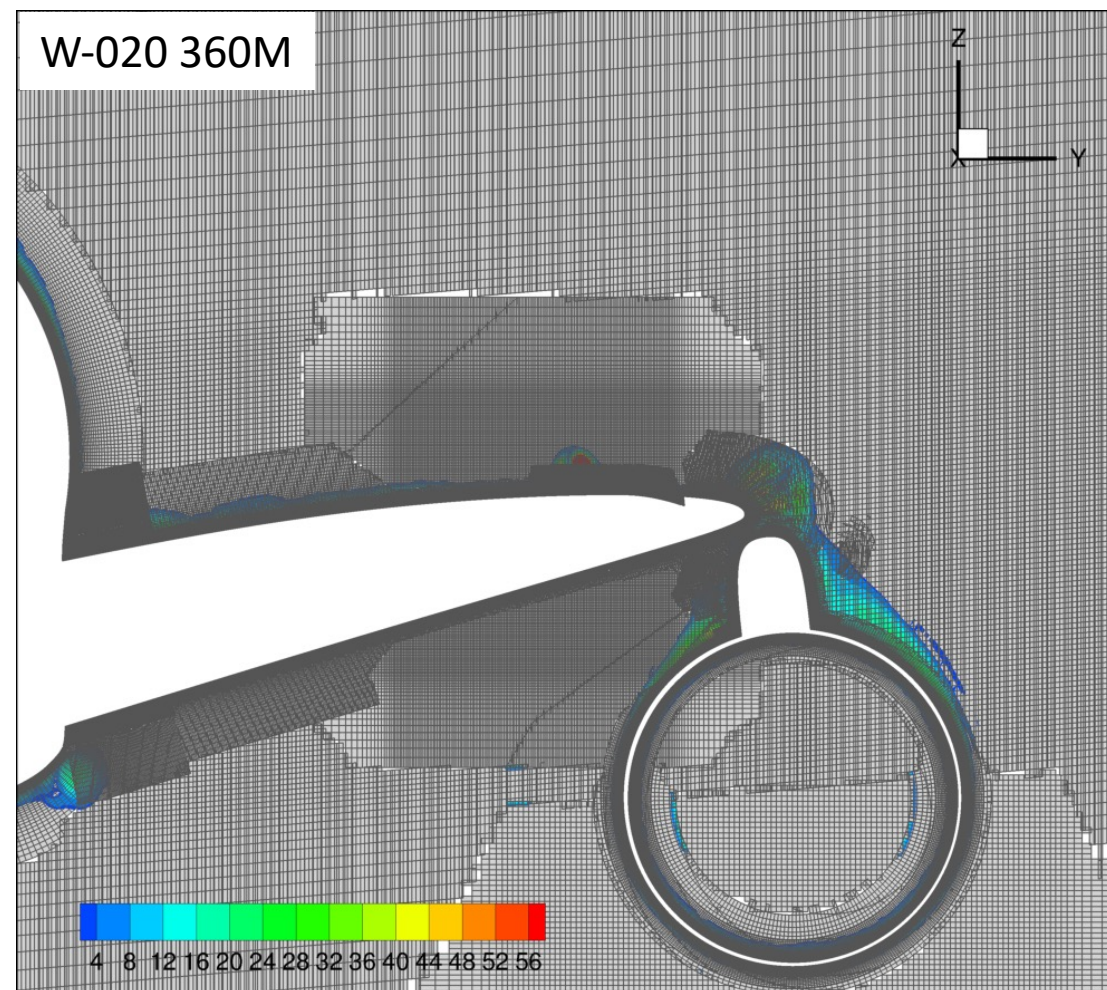
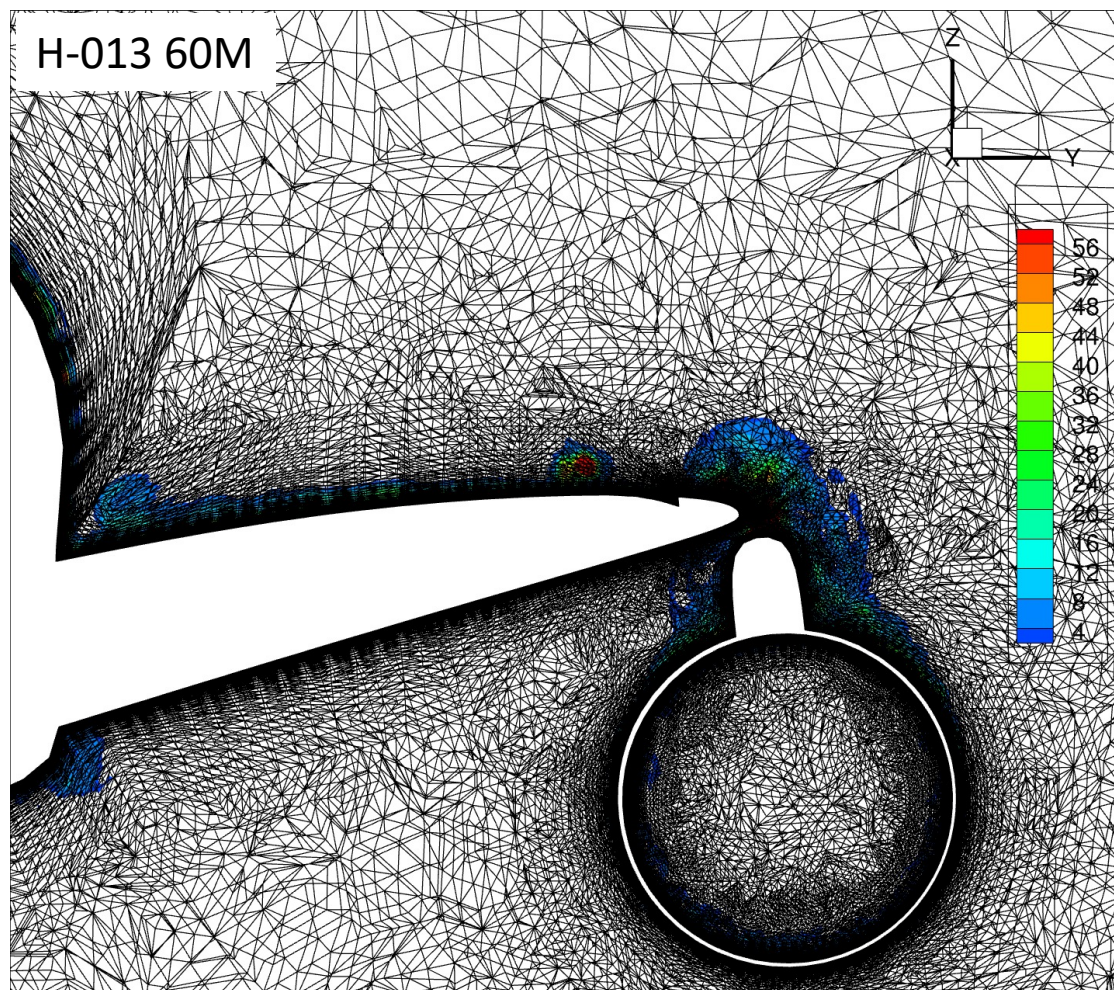


# ILES (7.05 AoA) View 12



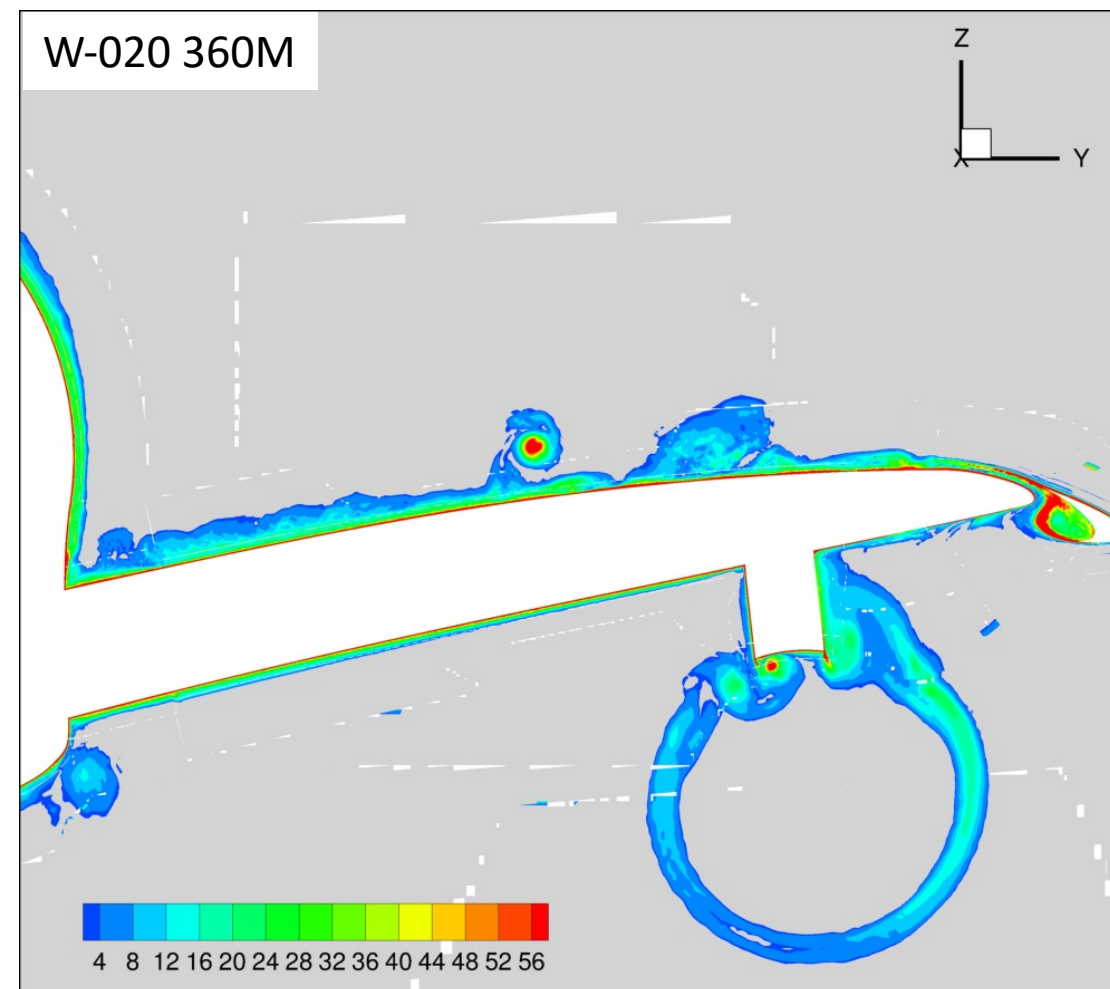
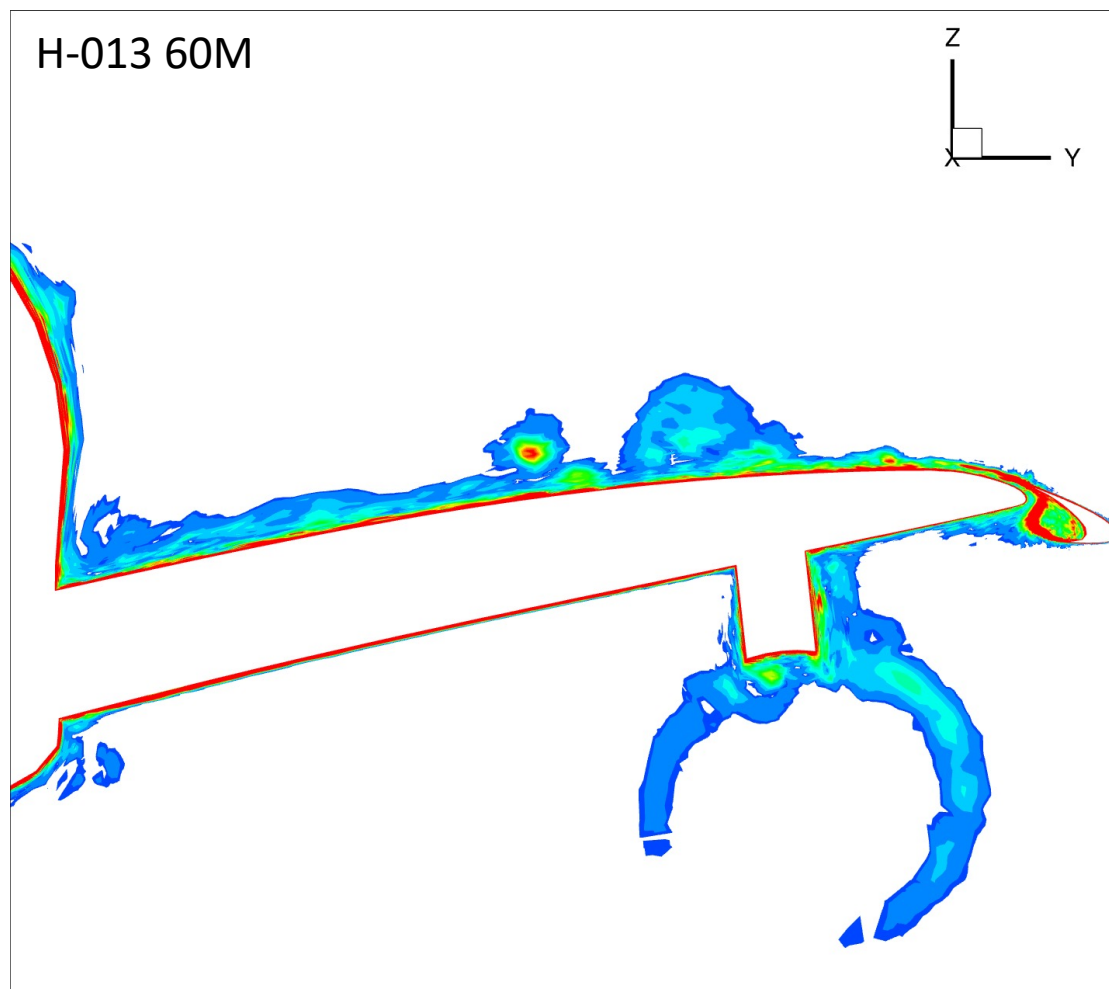


# ILES (7.05 AoA) View 12



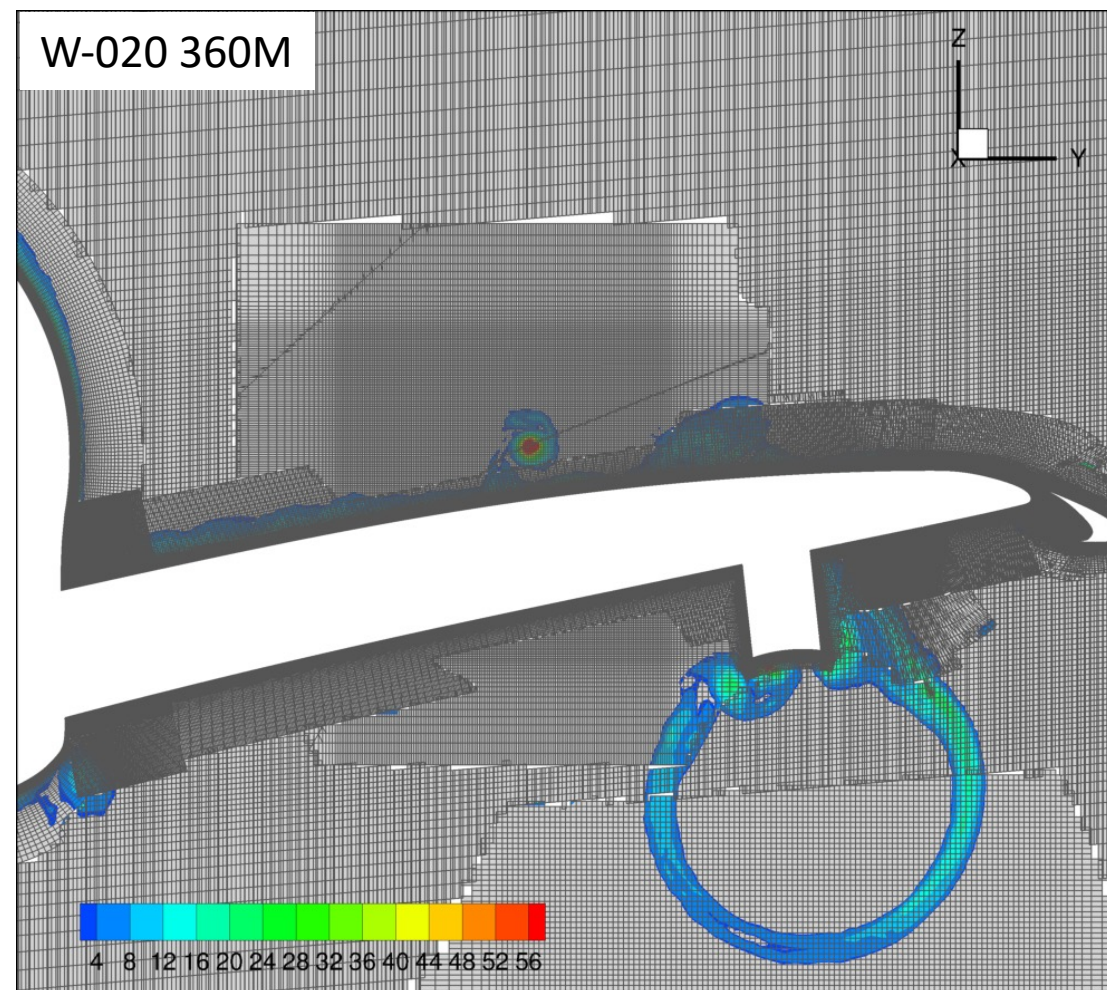
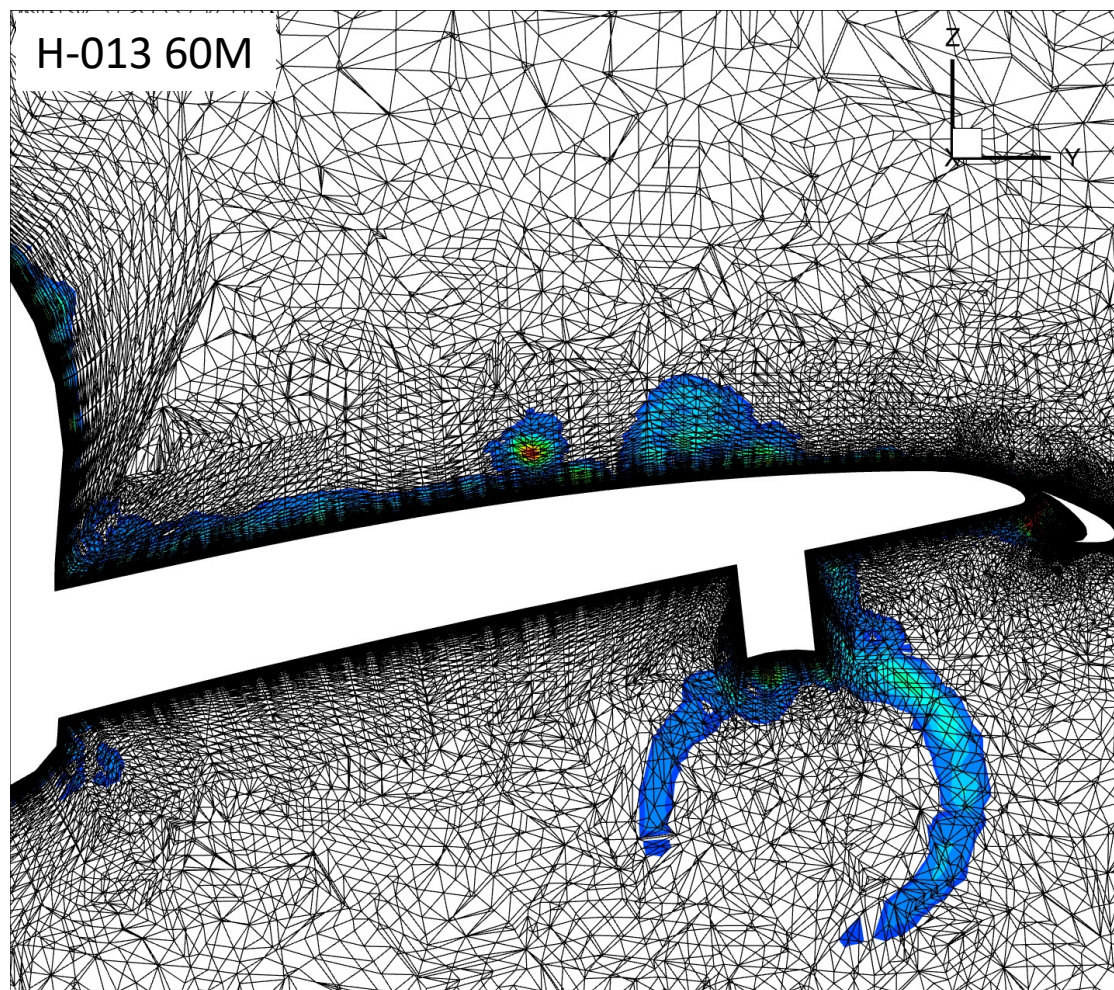


# ILES (7.05 AoA) View 13





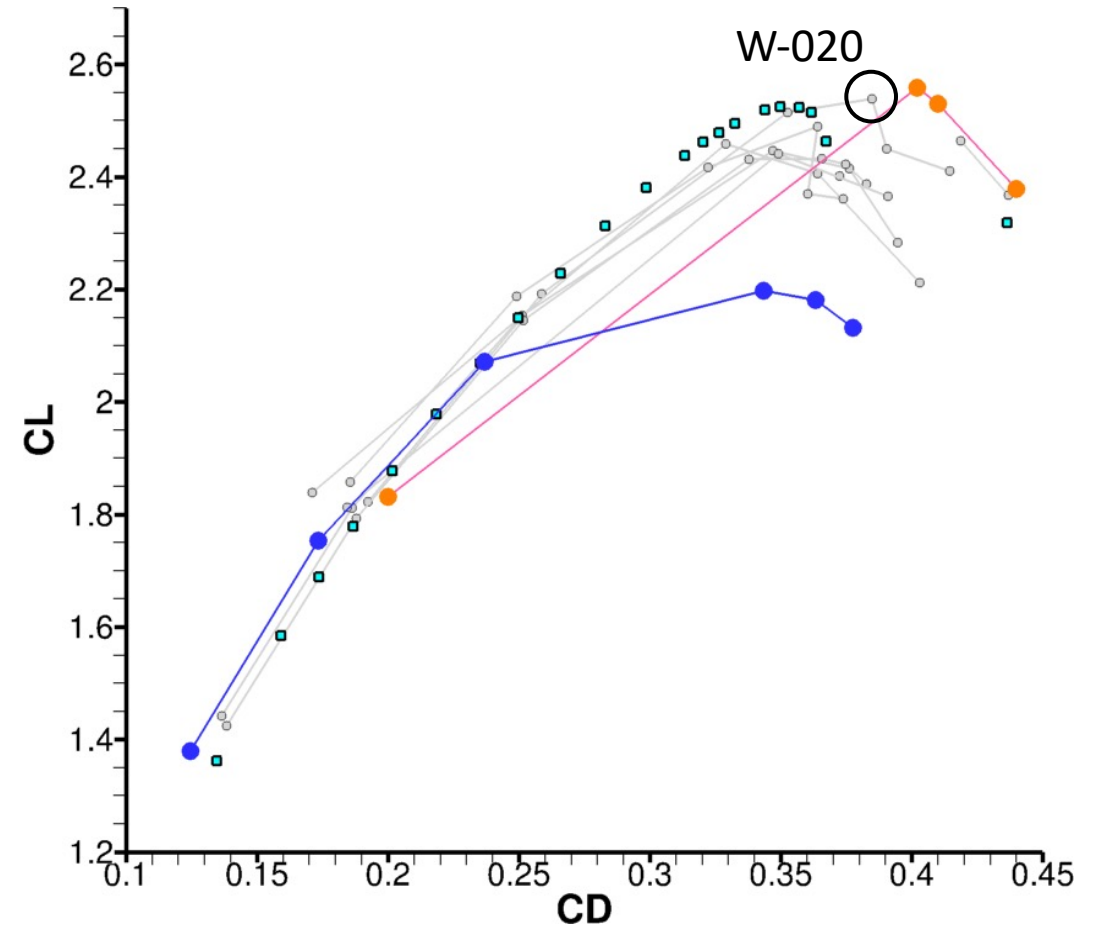
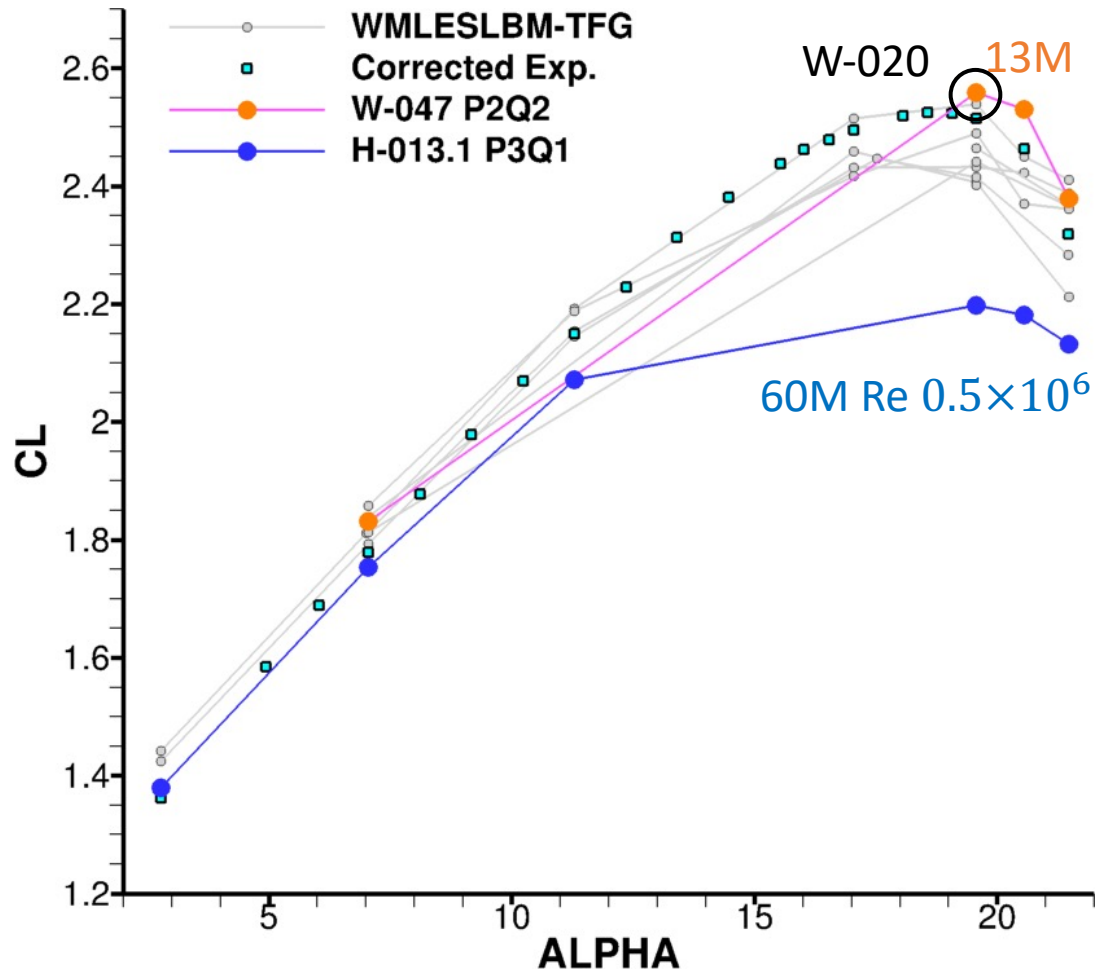
# ILES (7.05 AoA) View 13



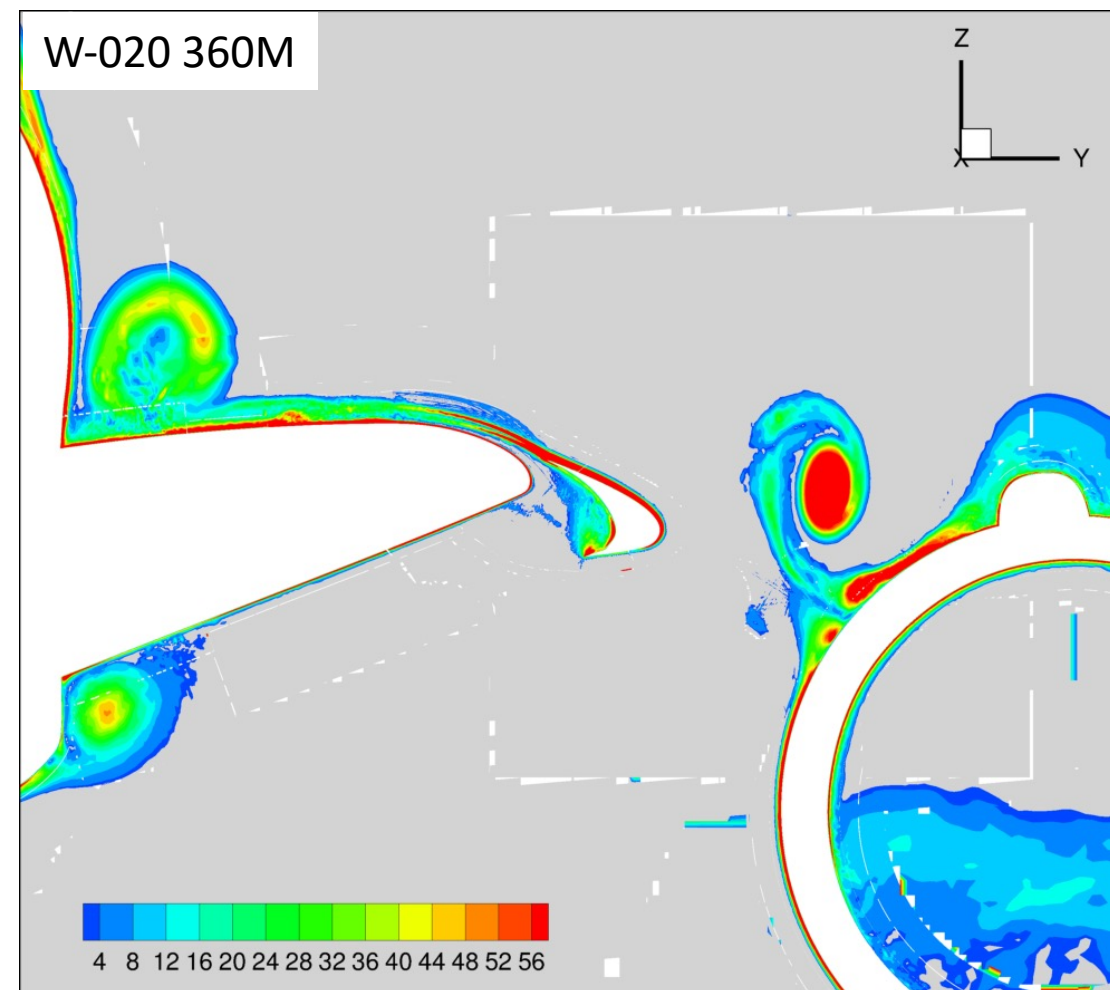
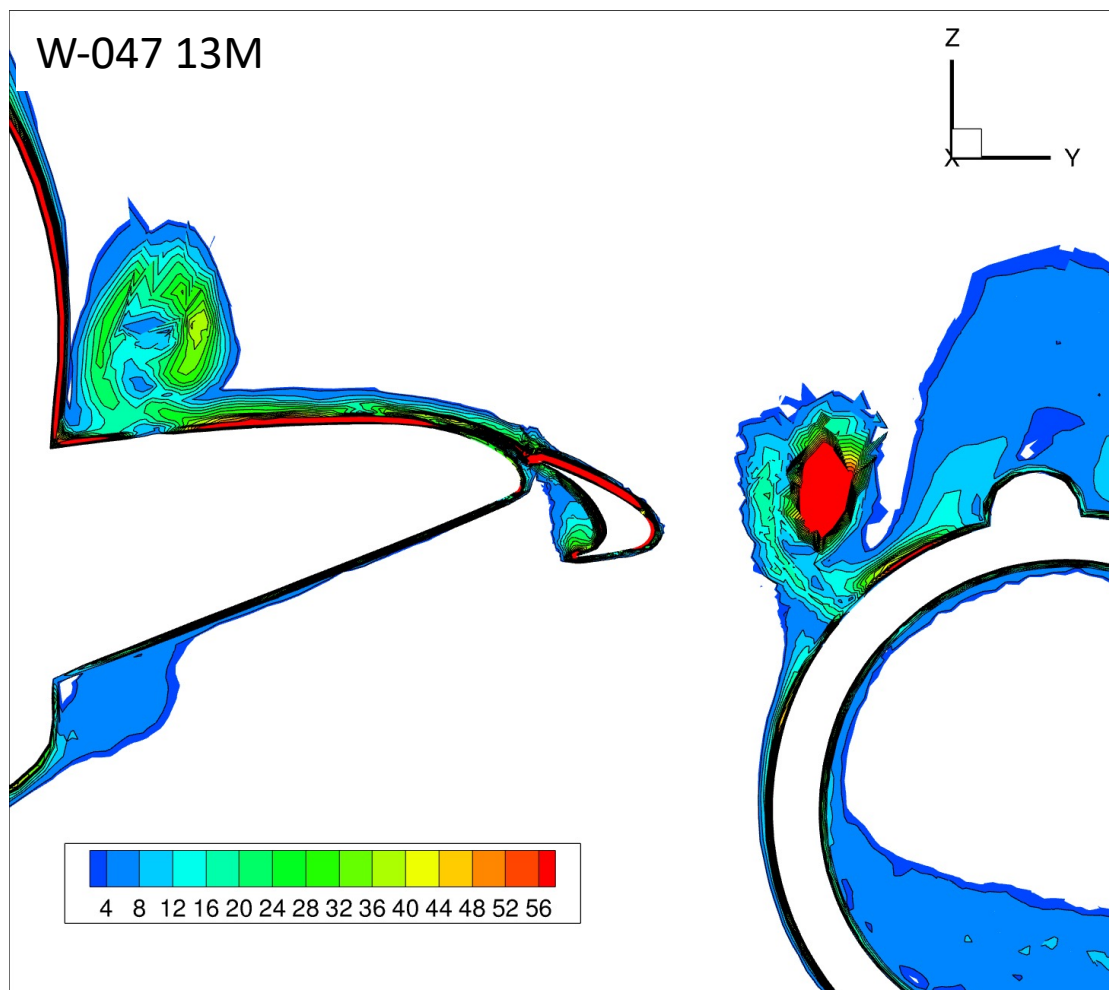


# Basic CFD Results Case2a

Lift curve ( $CL-\alpha$ ), drag polar ( $CL-CD$ ): LES

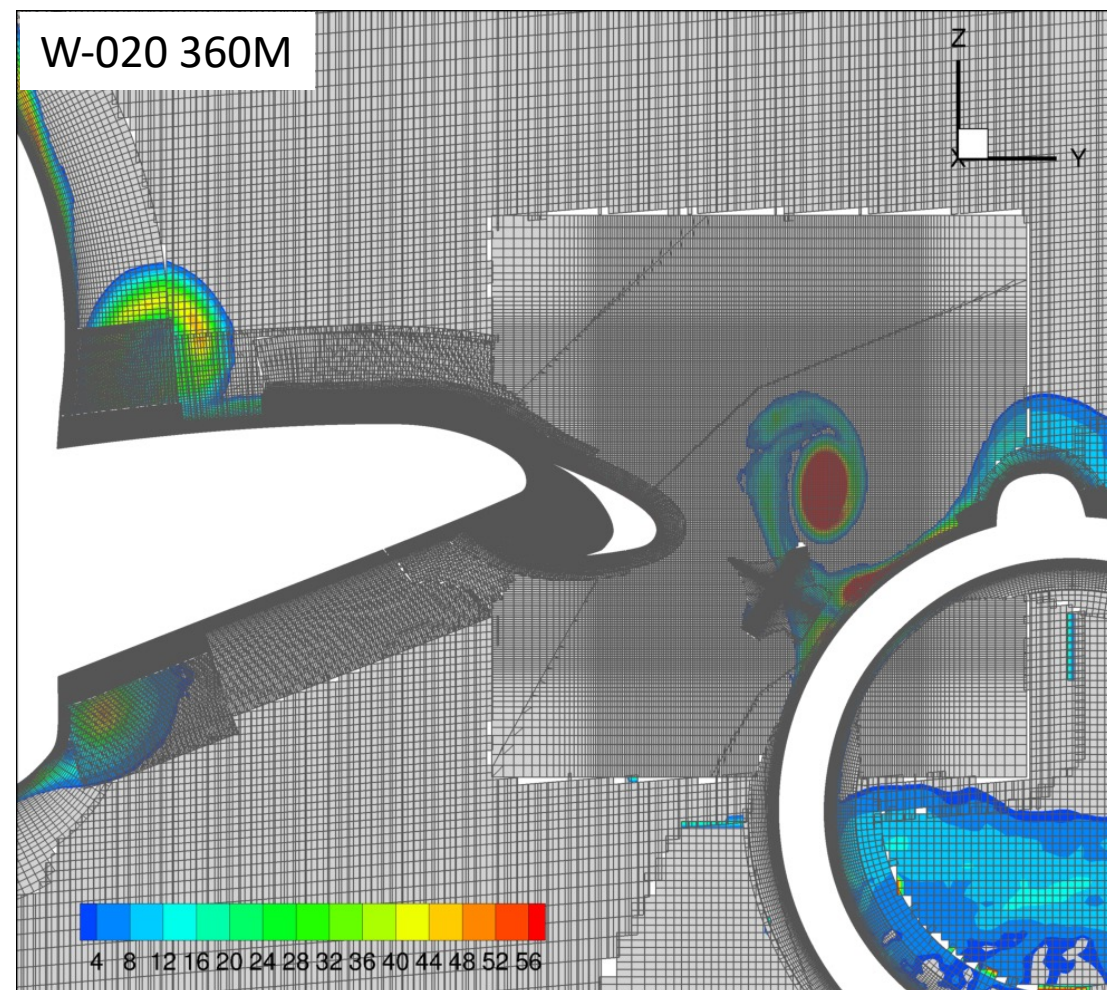
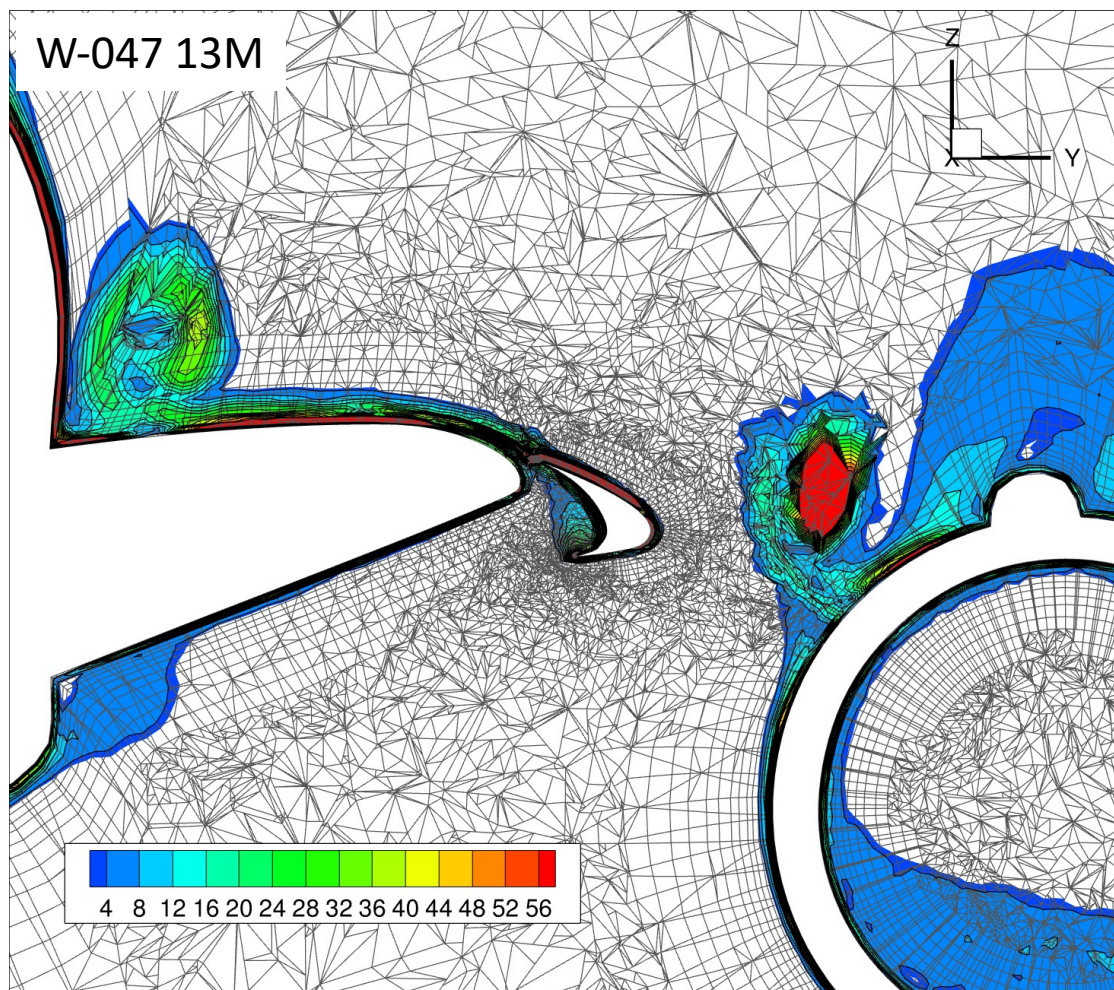


# WMLES (19.57 AoA) View 11



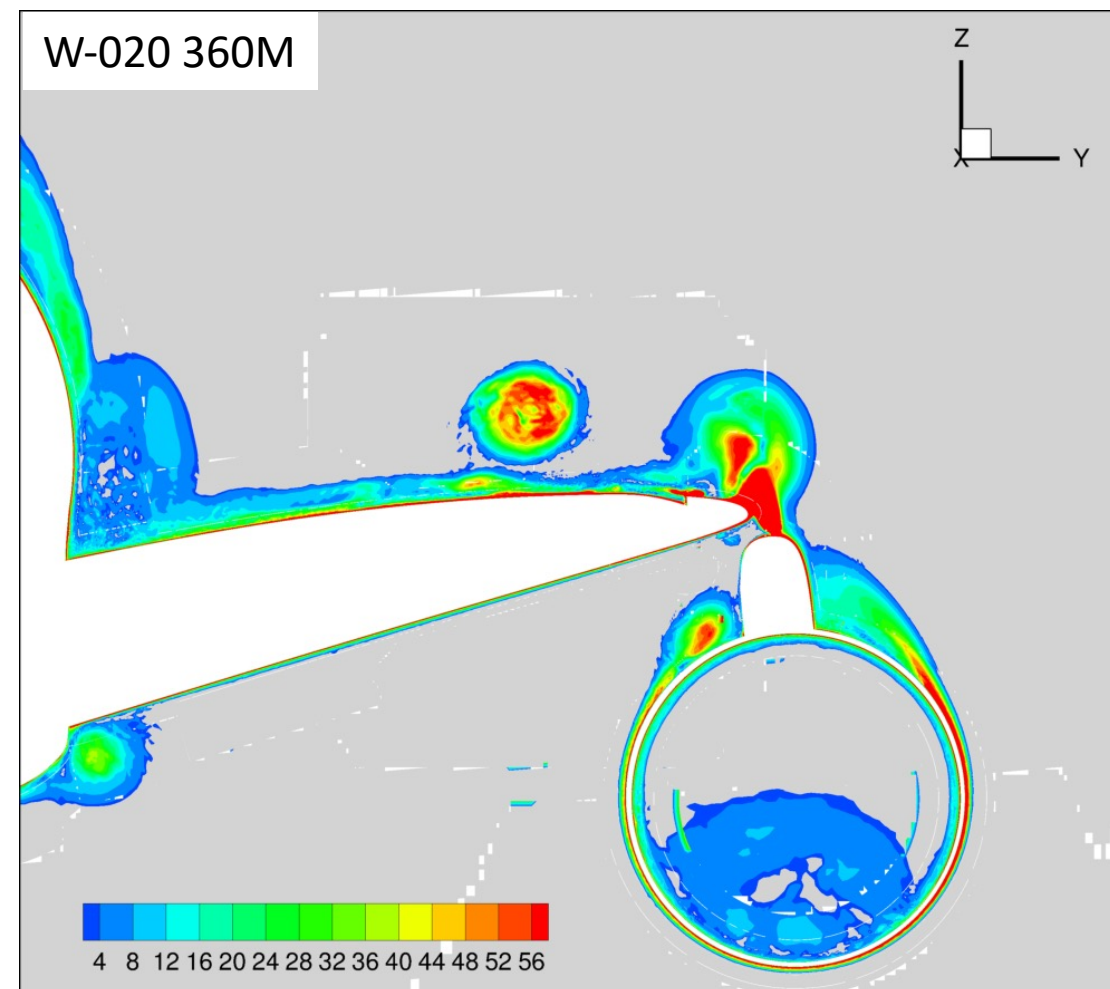
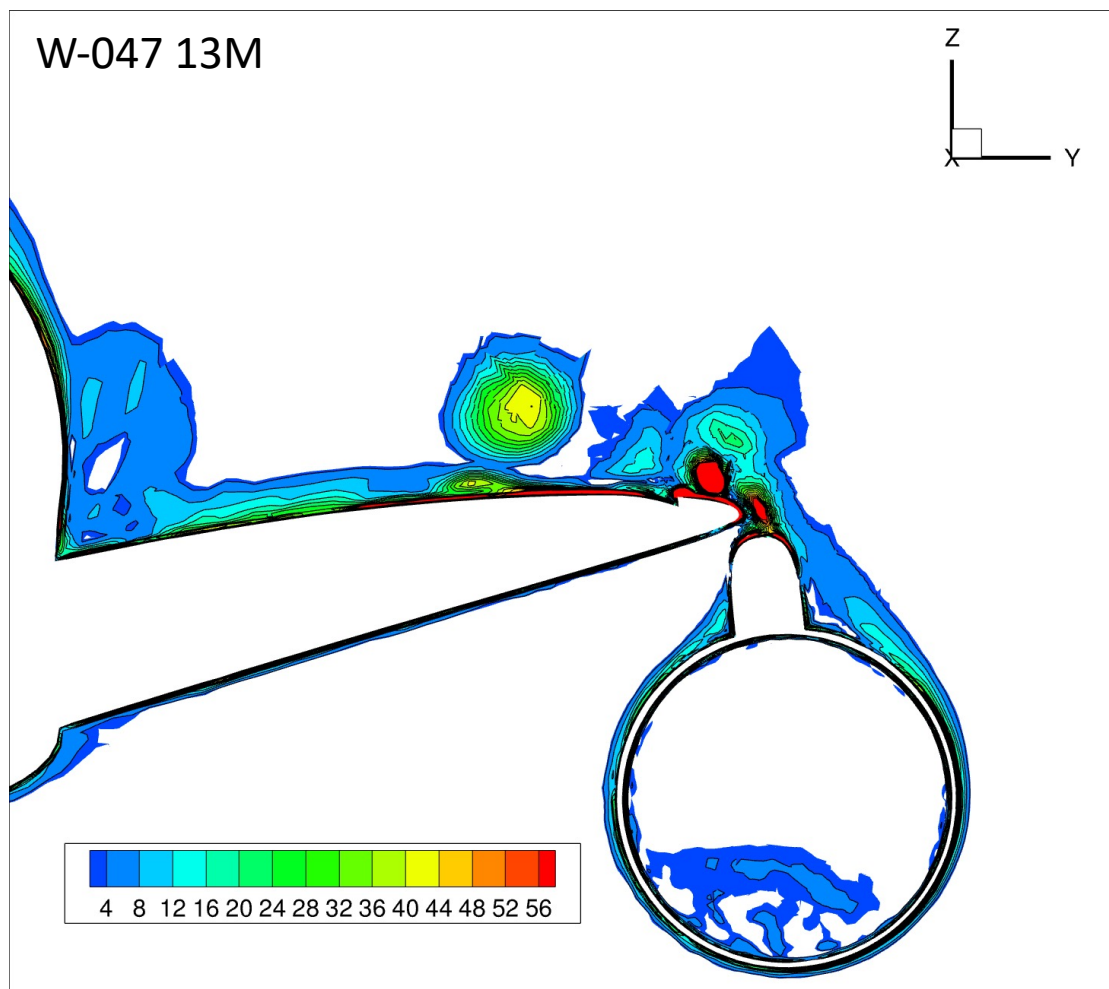


# WMLES (19.57 AoA) View 11



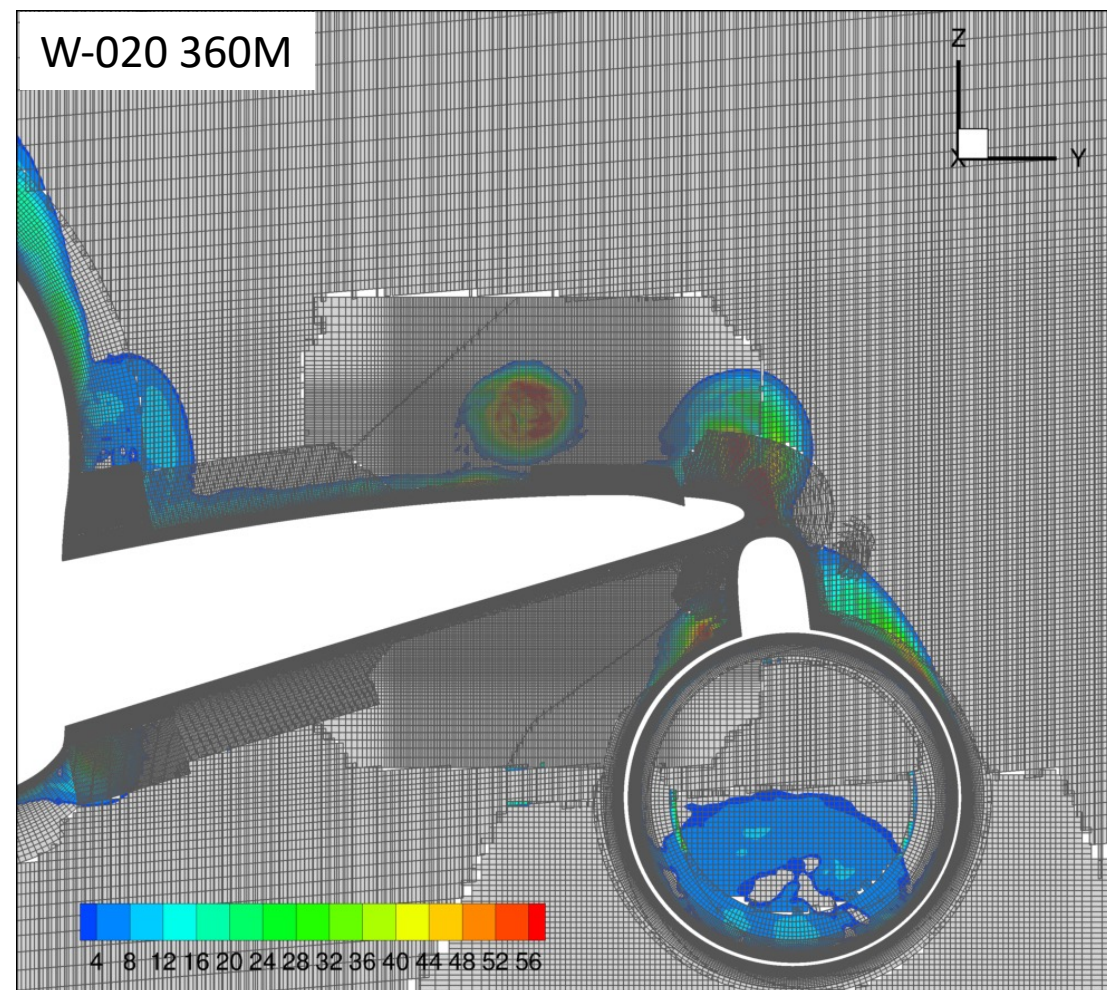
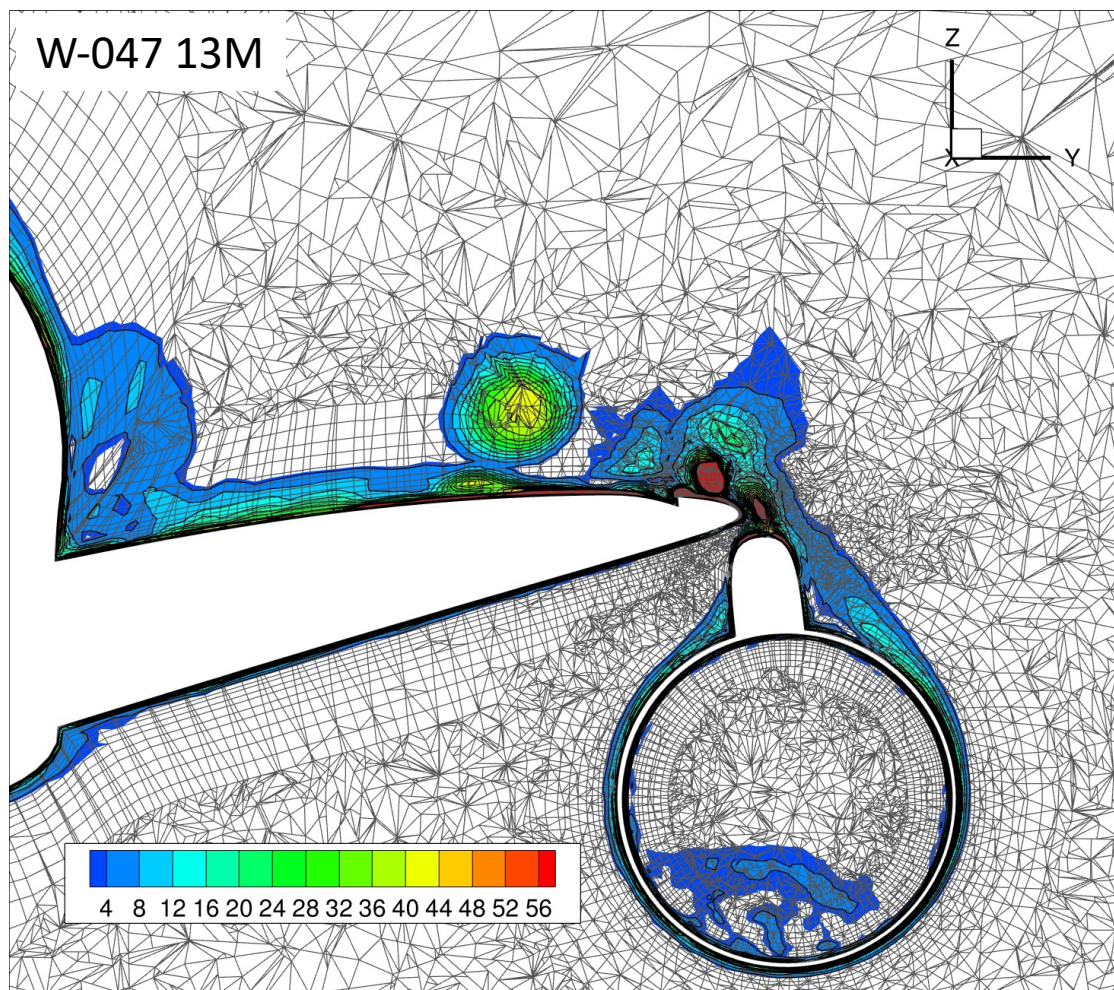


# WMLES (19.57 AoA) View 12



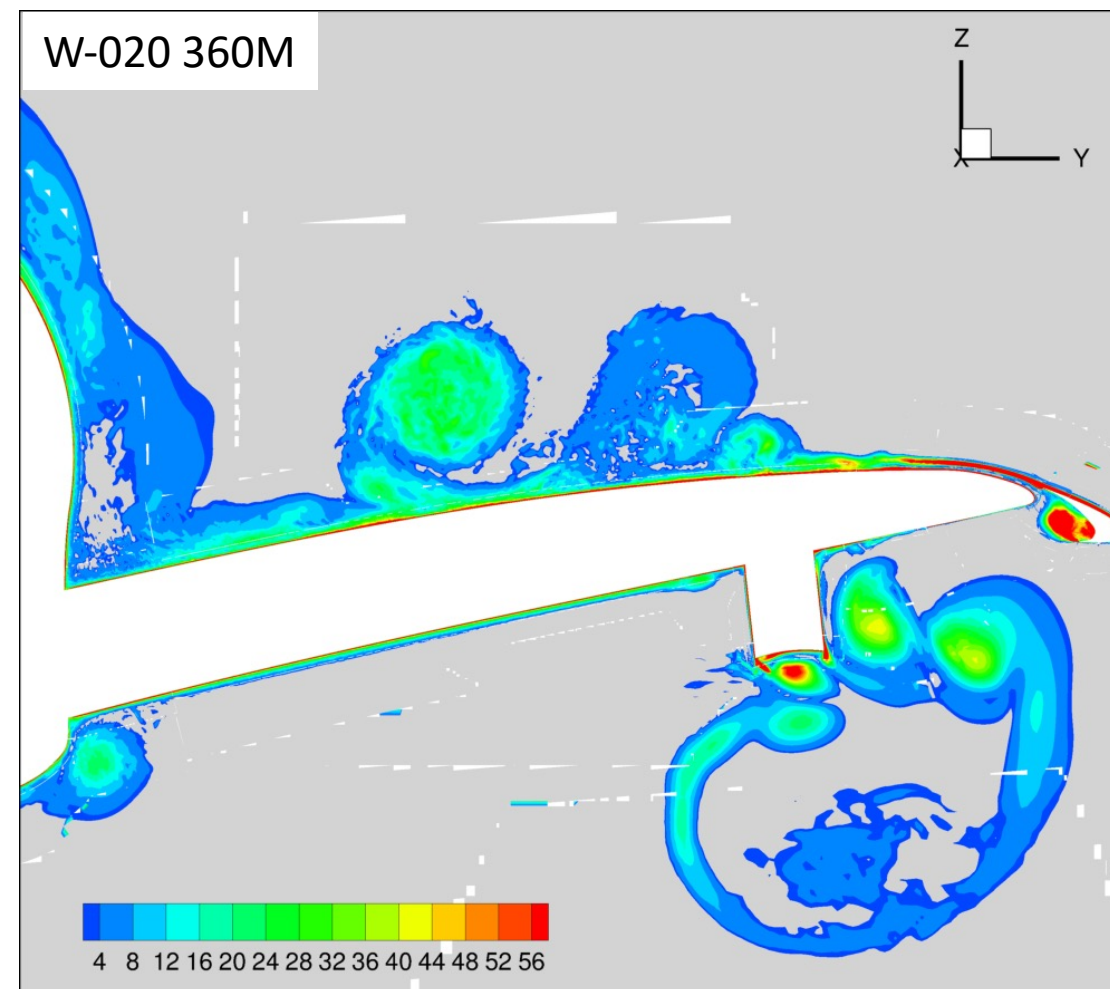
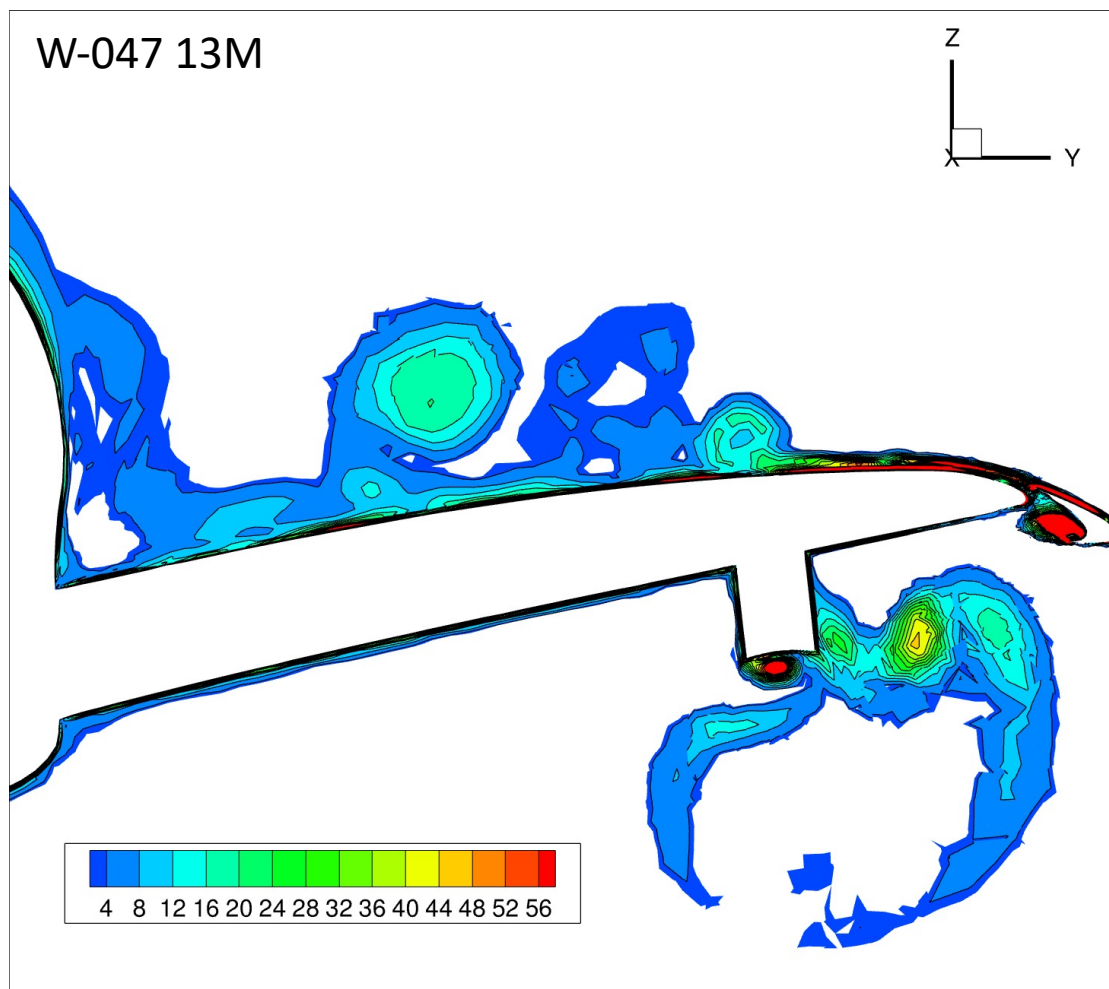


# WMLES (19.57 AoA) View 12



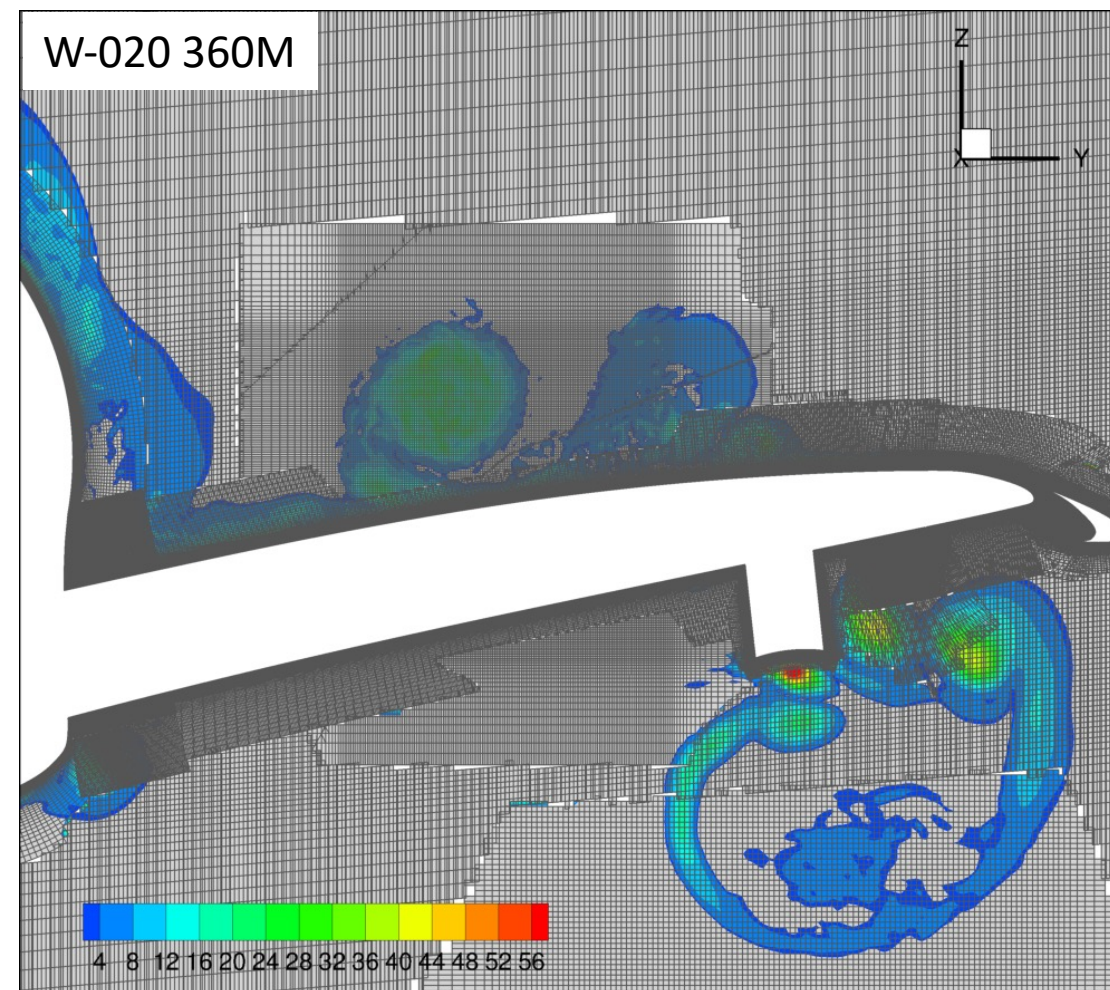
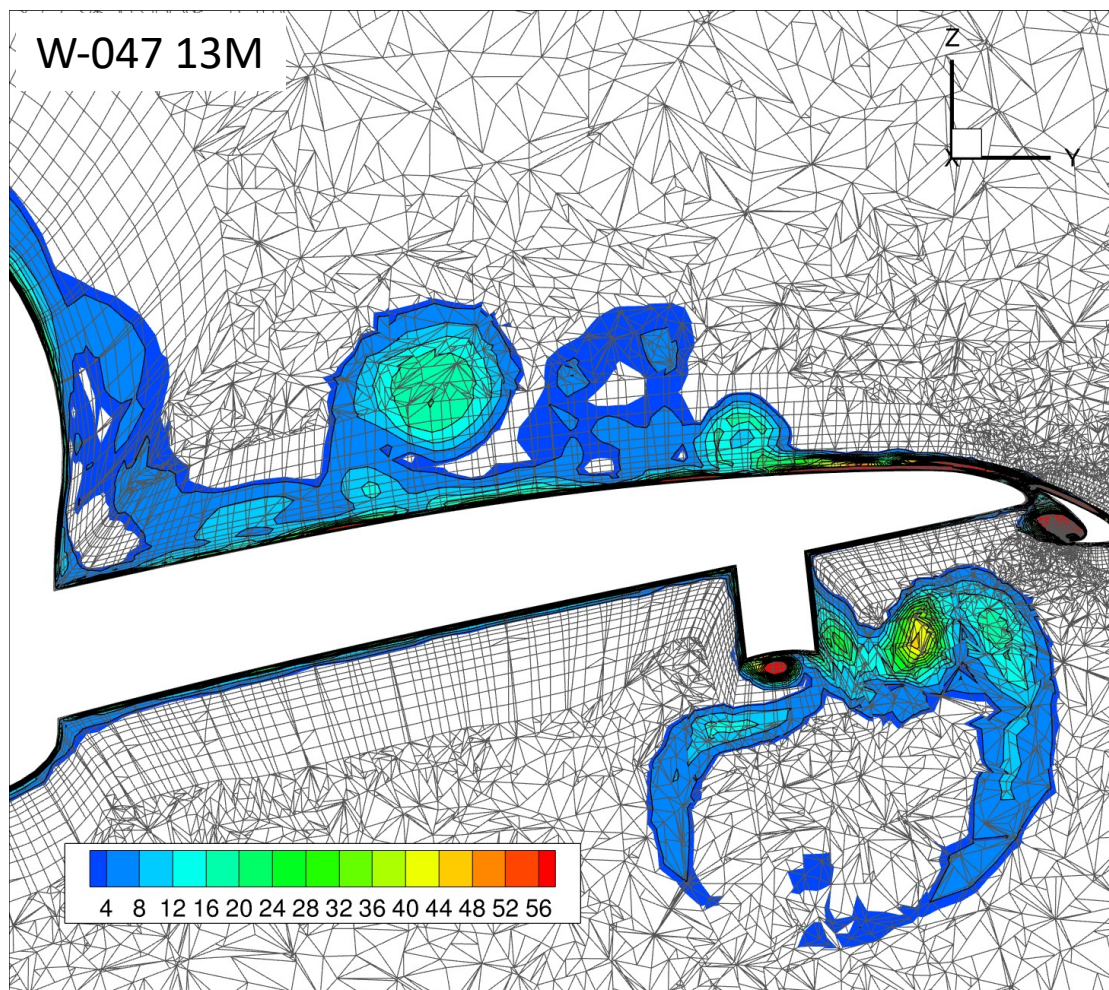


# WMLES (19.57 AoA) View 13



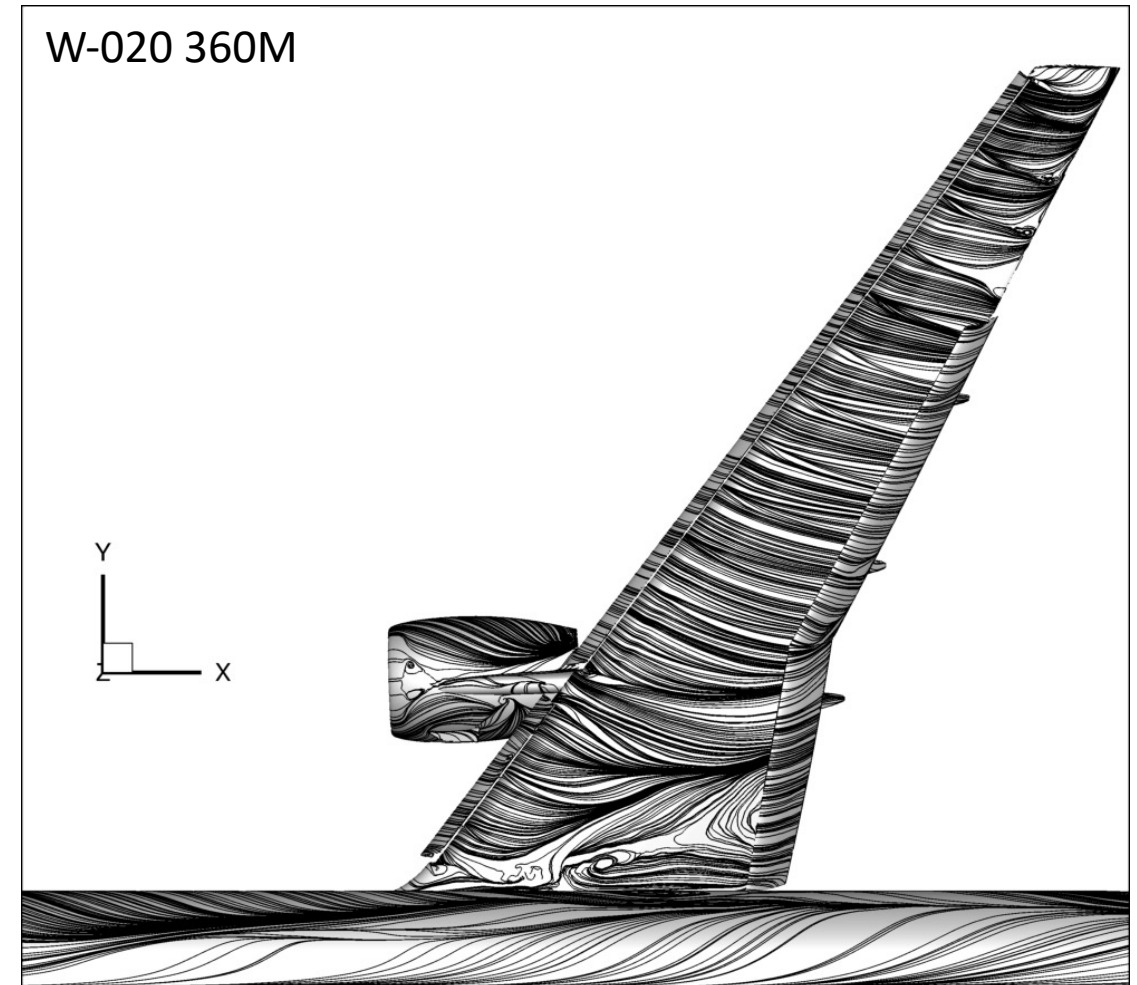
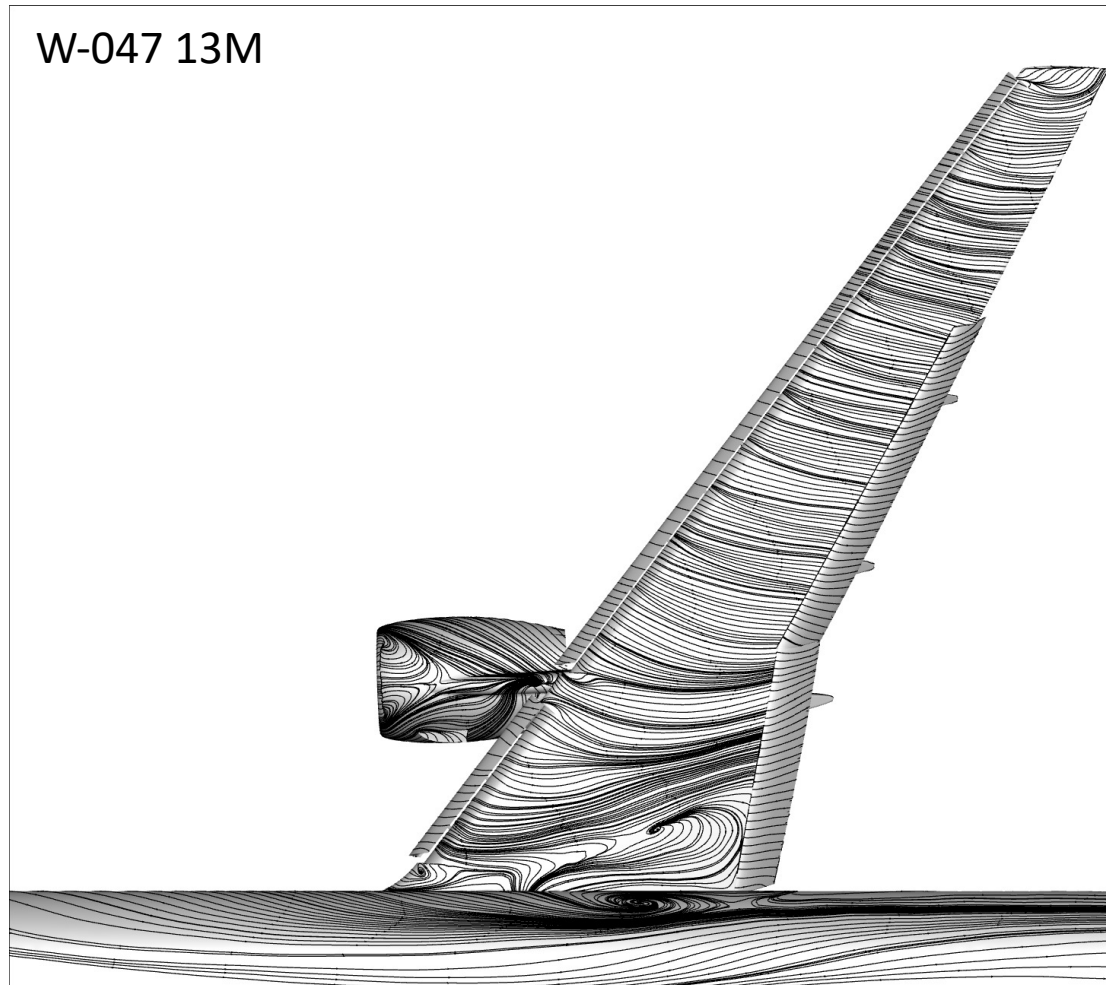


# WMLES (19.57 AoA) View 13

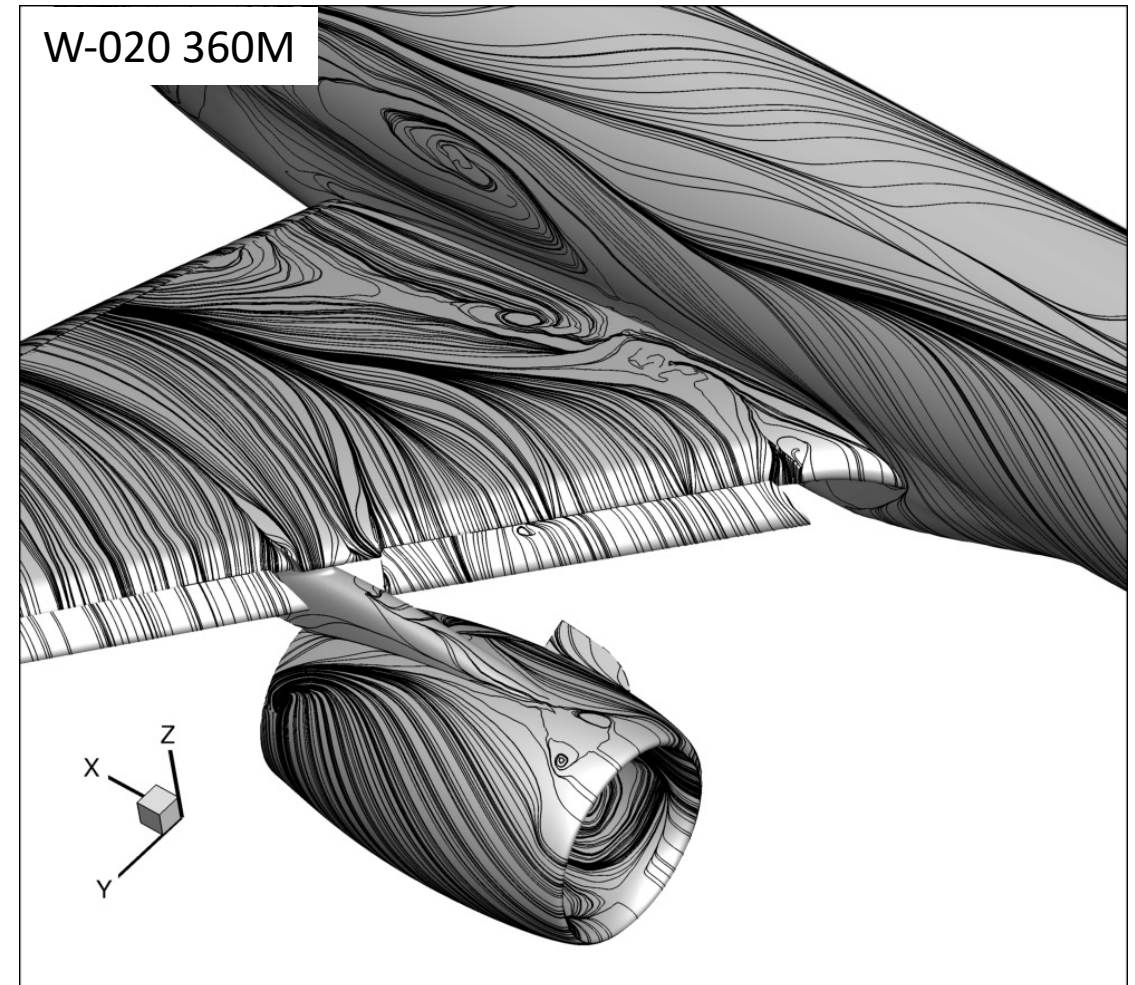
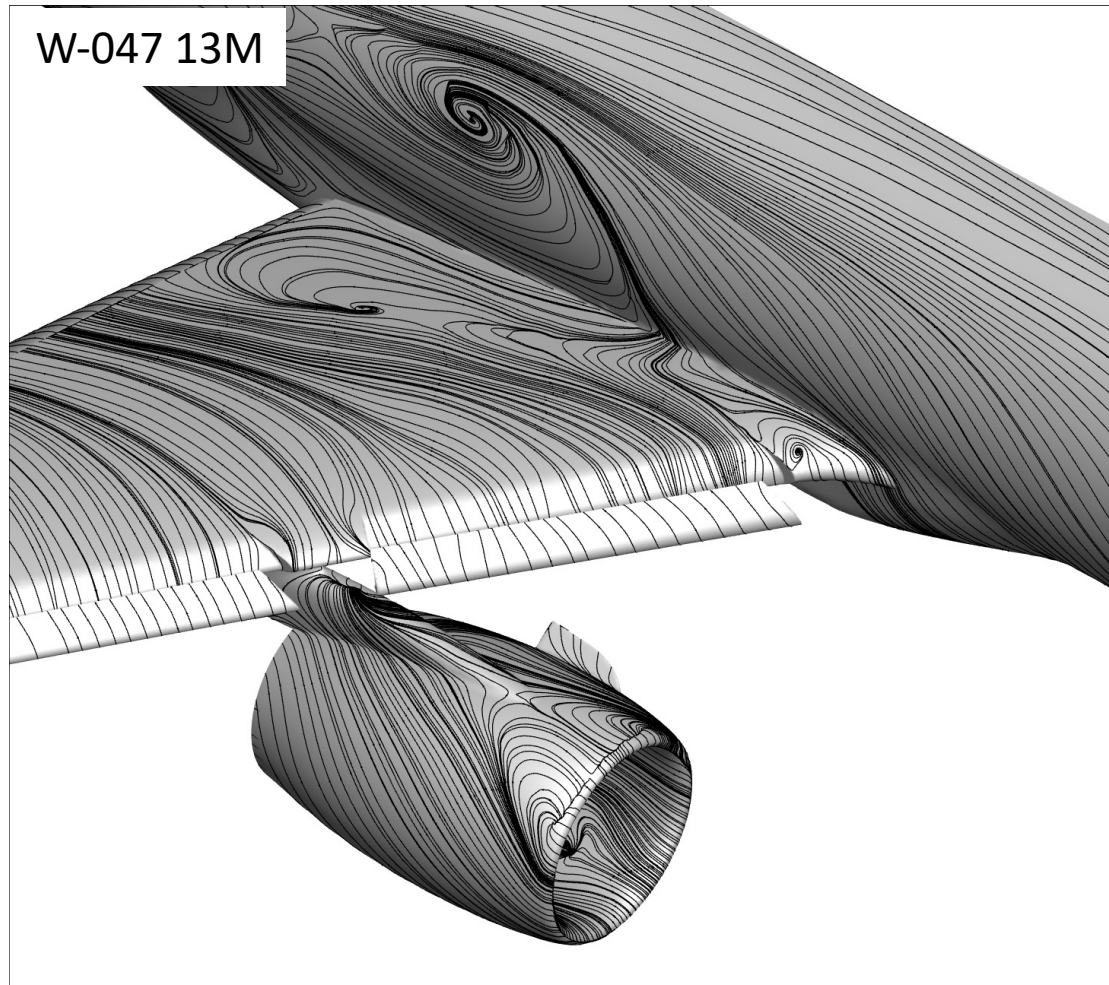




# WMLES (21.47 AoA) View 01



# WMLES (21.47 AoA) View 05





# W-047: (21.47 AoA) Oil-flows between $Y+ = 200$ (5mm) and $Y+ = 800$ (21 mm)

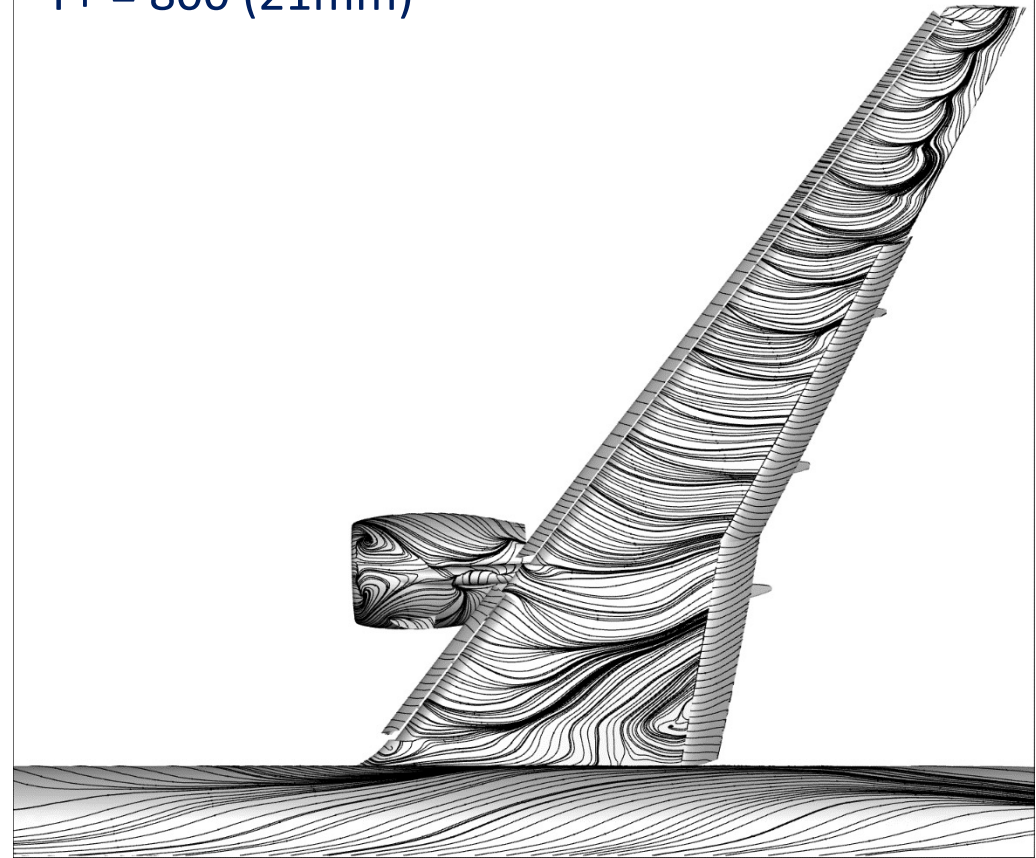
Same numerical setting at P2

Wall model data extracted between 1<sup>st</sup> and 2<sup>nd</sup> element off the wall

$Y+ = 200$  (5mm)



$Y+ = 800$  (21mm)



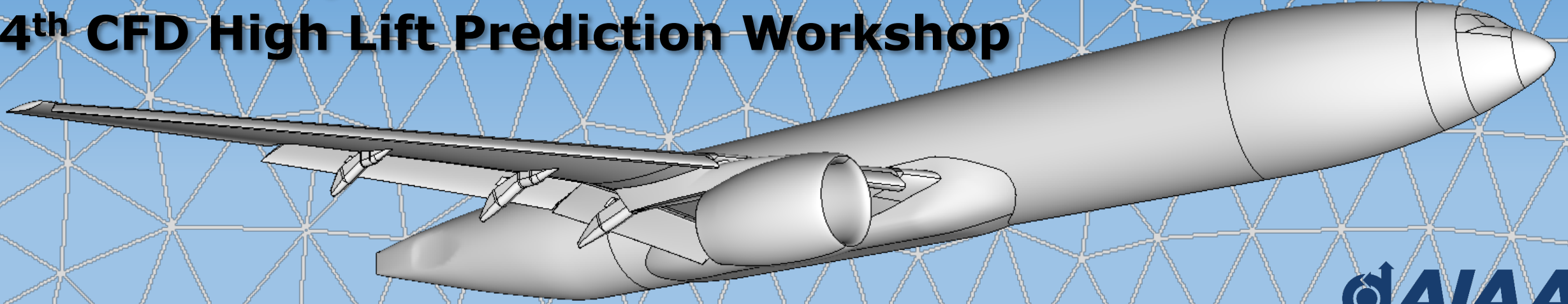


# Conclusions

- Higher order FEM/FV can be applied to HLCRM
  - Challenging, but doable
  - Mesh exchange issues
- Lots of learning for tuning linear solver settings, time steps, startup procedures (use explicit filtering)
- Implicit solvers are critical for high-order
  - Both RANS and LES calculations
- Mesh adaptation with high order promising in 2D
  - Mesh curving in 3D for highly-anisotropic elements is challenging
- WMLES P2 lift reasonable with only 13M DOF
  - Sensitive to wall element aspect ratio

# **3<sup>rd</sup> Geometry and Mesh Generation Workshop**

## **4<sup>th</sup> CFD High Lift Prediction Workshop**

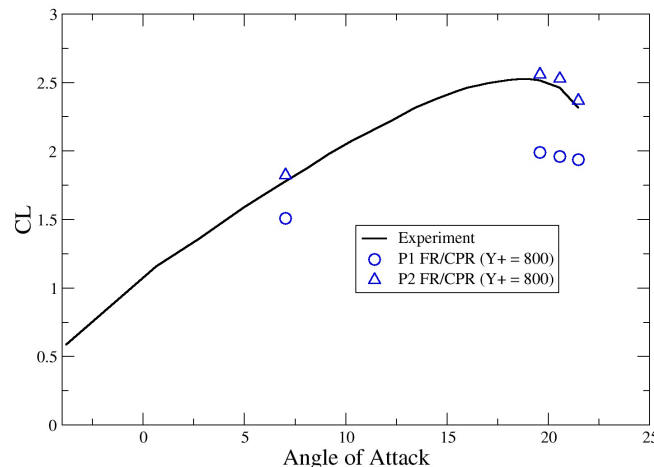


# **Backup**

# High-Order LES Case2a

## W-047

- P1 and P2 FR/CPR
- Optimized BDF2 with a GMRES solver
- Equilibrium wall-model
- Implicit LES
- Q2 mesh of 1.02M mixed (Pointwise  $Y^+ = 800$ )
  - P2 ~13.2 M DOF
  - Equivalent  $Y^+ \sim 200$ -260 near the wall (~7mm)



## H-013

- P3 DG
- BDF2 in time
  - Jacobian-free Newton-Krylov ILU(0)-GMRES
- No wall model
- Implicit LES ( $dt = 4.5e-5$ )
- **Q1** mesh 3M tet (Pointwise  $Y^+ = 100$ )
  - P3 60M DOF
- **$Re\ 0.5 \times 10^6$**